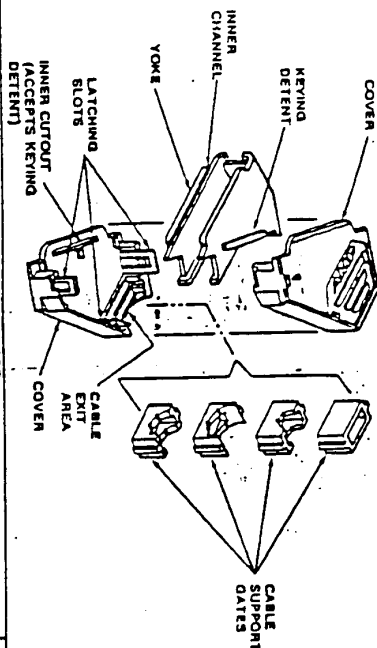




**AMP**  
AMP INCORPORATED  
HARRISBURG, PA 17108  
CUSTOMER HOTLINE  
1 800 722-1111

**AMP**  
AMP-20 AND HDE-20 CONNECTORS  
THREE-PIECE AND TWO-PIECE  
CABLE CLAMP KITS  
(STRAIGHT AND RIGHT-ANGLE)  
**IS 6659**  
RELEASED  
2-4-88

REDUCED FOR PACKAGING



PART NUMBERS					CONN TYPE
NO. OF CABLE CLAMP CON POSN	CABLE CLAMP CON ASSY	AMPLIMITE HDI-20 (Metal Shell) CONNECTORS	AMPLIMITE HDE-20 (Metal Shell) CONNECTORS	AMPLIMITE HDE-20 (All-Plastic) CONNECTORS	
23	745306	205308	745486	745211	Plug
		207484			
		205438			
		206307	745436	745304	Repl
		207483			
37	745311	205441	745498	745215	Plug
		205310			
		205437			
		205308	745497	745313	Repl
		205442			

**1. INTRODUCTION**

This instruction sheet (IS) covers the assembly and specification procedures for AMP-20 and HDE-20 connectors. The three-piece cable clamp kits, as they contain parts manufactured from black thermoplastic material. The three-piece kits are designed for the AMP-20 and HDE-20 connectors listed in Figure 1. The

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IS 6659

## 2. DESCRIPTION

Three-piece kits 745306 and 745311 can be used in either 80° (right-angle) or 180° (straight) cable-clamp applications. Each three-piece kit features a yoke, two mating covers, and cable support gates. The yokes contained in kits 745306 and 745311 feature inner channels which slide onto the connector flange during assembly. The yoke also has two latching detents to accept the inner channels of the covers. Each cover features three latching areas and a cable-exit area. One cover has latching slots which are secured to the latching tabs of the other cover. Each cover also has a built-in inner cutoff which snaps over the detent base of the yoke. The cable-exit areas will accept one of the four available cable support gates supplied with the kit.

Except for kit 745550, each two-piece kit features two cable support gates and a cable support gate. Kit 745550 consists of two covers with "built-in" cable support gates. Two-piece kit 745547, 745553, and 745560 are designed for 180° cable-clamp applications only and kit 745550 is used with 80° cable-clamp applications only. Two-piece kits have the same latching features as the three-piece kits; one cover has latching slots which are secured to the latching tabs of the other cover.

The cable support gates are designed to restrict the aperture diameter of the cable and area depending on the diameter of the cable or wire bundle being used. The cable support gates should provide sufficient clearance of the cable exit areas to provide sufficient clearance for the cable to exit the connector flange. The cable-exit areas of kits 745306, 745311, and 745560 will accommodate discrete wires or latched

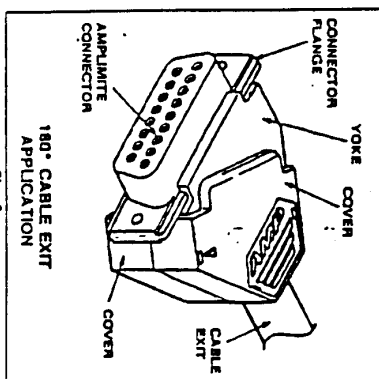


Fig. 2

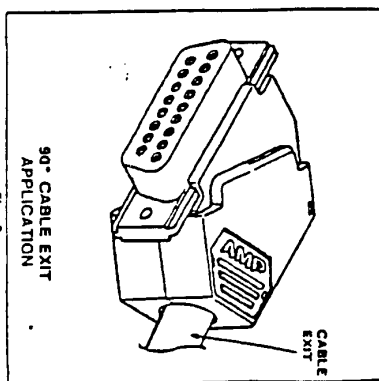


Fig. 3

AMPLIMITE CABLE CLAMP KITS

cable up to .500 in. in diameter. The cable-exit area of kits 745547 and 745550 will accommodate up to .310 in. in diameter and the cable-exit area of kit 745553 will accommodate up to .425 in. in diameter.

## NOTE

If you are using a three-piece kit, follow the procedures in Sections 3 and 5. If you are using a two-piece kit, proceed to Sections 4 and 5.

## 3. ASSEMBLY PROCEDURE, THREE-PIECE KITS

Determine that you have the correct cable clamp kit for the connector you are using. Then proceed as follows:

1. Terminate the conductors in the connector you are using according to the instructions packaged with the tooling.

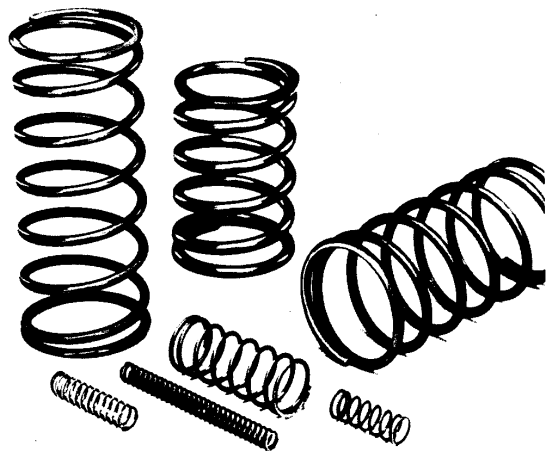
## NOTE

Ensure that you maintain 1-in. length on individual conductors when using jacketed cable.

2. Slide the yoke onto the connector flange.
3. Lay the cover with the latching slots on a flat surface with the slots in an upright position. See Figure 1.
4. Depending on the cable-exit orientation you desire (left or right angle), lay the yoke and connector assembly in the cover. See Figures 2 and 3.

PAGE 2 OF 4

# Compression Springs



## Stock sizes in music wire and stainless steel

Associated Spring offers a broad variety of helical compression springs in the SPEC selection. They are reliable, inexpensive and efficient — the right combination for general-purpose use throughout industry.

### Material

#### Music wire

ASTM-A228 or AMS 5112

#### Stainless steel

Commercial Type 302, ASTM-A313 or AMS 5688 spring temper. (chemical & physical only)

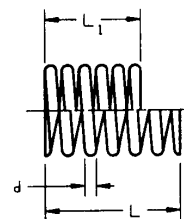
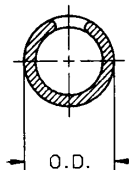
No charge for certificate of compliance when requested; certificate of chemical analysis available, see price book.

Music wire will be furnished unless stainless steel is specified. When inquiring or ordering, use letter "M" or letter "S" as suffix on catalog numbers to designate music wire or stainless steel wire, respectively.

Music wire springs are not recommended for applications where the temperature exceeds 250 deg F (121 deg C). Stainless steel springs are not recommended for applications where the temperature exceeds 500 deg F (260 deg C).

For normal service, springs should not be compressed below  $L_1$ .

To determine load  $P$  at any length other than  $L_1$ , multiply the proposed deflection by the rate  $R$ .  $*[P + (L - L_x) \times R]$  When stainless steel is used the value for rate  $R$  must be corrected by multiplying  $R$  by 0.833.



### Direction of Helix

Right hand.

### Ends

Squared and ground. Ends to be square within 3° with axis. O.D. sizes 0.057-0.088 in (1.45-2.24 mm) squared ends not ground.

Free length  $L$  is for reference use only. Load  $P$  is attained at length  $L_1$ . For stainless steel multiply  $P$  by 0.833.

Load values shown are for music wire.

### Finishes

Standard finish is that of the normal wire. Shot-peened and plated finishes furnished on request. Allow sufficient additional time for special finishes.

### Tolerances

O.D. (English)	O.D. (Metric)
0.057 to 0.119 in $\pm$ 0.003 in	1.45 to 3.02 mm $\pm$ 0.08 mm
0.120 to 0.240 in $\pm$ 0.005 in	3.05 to 6.10 mm $\pm$ 0.13 mm
0.241 to 0.500 in $\pm$ 0.008 in	6.12 to 12.70 mm $\pm$ 0.20 mm
0.501 to 1.000 in $\pm$ 0.015 in	12.73 to 25.40 mm $\pm$ 0.38 mm
1.001 to 1.225 in $\pm$ 0.020 in	25.43 to 31.12 mm $\pm$ 0.51 mm
1.226 to 1.460 in $\pm$ 0.030 in	31.14 to 37.08 mm $\pm$ 0.76 mm
1.461 to 2.000 in $\pm$ 0.040 in	37.11 to 50.80 mm $\pm$ 1.02 mm

Load,  $P \pm 10\%$   
Spring Rate,  $R \pm 10\%$

\* $L_x$  = Desired Load Length

# THE 1999 FIRST ROBOTICS COMPETITION MANUAL

## STOCK COMPRESSION SPRINGS Music Wire and Stainless Steel



Associated Spring  
Raymond BARNES

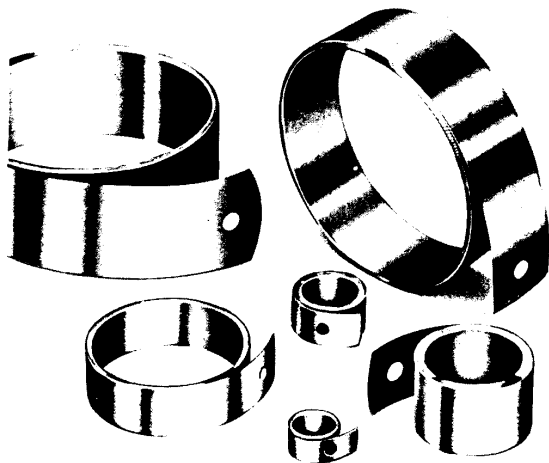
CATALOG NUMBER*	Outside Diameter		Wire Diameter		Free Length L, Approx.		Load, P at L <sub>1</sub>		Length, L <sub>1</sub>		Solid Height, Approx.		Spring Rate, R	
	in	mm	in	mm	in	mm	lb†	N†	in	mm	in	mm	lb/in†	N/mm†
C0600-063-2000	0.600	15.24	0.063	1.60	2.00	50.80	18.00	80.07	1.059	26.90	0.700	17.78	18.0	3.15
C0600-063-2250					2.25	57.15			1.184	30.07	0.768	19.51	15.9	2.78
C0600-063-2500					2.50	63.50			1.308	33.22	0.836	21.23	14.2	2.49
C0600-063-2750					2.75	69.85			1.433	36.40	0.863	21.92	13.7	2.40
C0600-063-3000					3.00	76.20			1.558	39.57	0.927	23.55	12.5	2.19
C0600-063-3500					3.50	88.90			1.807	45.90	1.055	26.80	10.6	1.856
C0600-067-0625			0.067	1.70	0.62	15.75	21.00	93.41	0.360	9.14	0.300	7.62	80.0	14.01
C0600-067-0750					0.75	19.05			0.430	10.92	0.336	8.53	66.0	11.56
C0600-067-0880					0.88	22.35			0.455	11.56	0.401	10.19	50.0	8.76
C0600-067-1000					1.00	25.40			0.530	13.46	0.430	10.92	45.0	7.88
C0600-067-1250					1.25	31.75			0.665	16.89	0.505	12.83	36.0	6.30
C0600-067-1500					1.50	38.10			0.780	19.81	0.594	15.09	29.0	5.08
C0600-067-1750			1.75	44.45	0.830	21.08	0.715	18.16	23.0	4.03				
C0600-067-2000			2.00	50.80	1.106	28.09	0.771	19.58	22.5	3.94				
C0600-067-2250			2.25	57.15	1.236	31.39	0.847	21.51	19.8	3.47				
C0600-067-2500			2.50	63.50	1.366	34.70	0.923	23.44	17.7	3.10				
C0600-067-2750			2.75	69.85	1.496	38.00	0.966	24.54	16.7	2.92				
C0600-067-3000			3.00	76.20	1.626	41.30	1.040	26.42	15.3	2.68				
C0600-072-0620			0.072	1.83	0.62	15.75	24.00	106.76	0.405	10.29	0.381	9.68	114.5	20.05
C0600-072-0750					0.75	19.05			0.445	11.30	0.396	10.06	78.0	13.66
C0600-072-0880					0.88	22.35			0.520	13.21	0.433	11.00	68.0	11.91
C0600-072-1000					1.00	25.40			0.565	14.35	0.502	12.75	55.0	9.63
C0600-072-1250					1.25	31.75			0.710	18.03	0.581	14.76	45.0	7.88
C0600-072-1500					1.50	38.10			0.830	21.08	0.691	17.55	36.0	6.30
C0600-072-1750			1.75	44.45	0.950	24.13	0.801	20.35	30.0	5.25				
C0600-072-2000			2.00	50.80	1.140	28.96	0.848	21.54	28.0	4.90				
C0600-072-2250			2.25	57.15	1.301	33.05	0.946	24.03	25.9	4.54				
C0600-072-2500			2.50	63.50	1.438	36.53	1.033	26.24	23.1	4.05				
C0600-072-2750			2.75	69.85	1.601	40.67	1.119	28.42	20.9	3.66				
C0600-072-3000			3.00	76.20	1.742	44.25	1.206	30.63	19.1	3.34				
C0600-081-0620			0.081	2.06	0.62	15.75	32.69	145.41	0.466	11.84	0.412	10.46	212.6	37.23
C0600-081-0750					0.75	19.05			0.553	14.05	0.459	11.66	165.6	29.00
C0600-081-0880					0.88	22.35			0.639	16.23	0.507	12.88	135.6	23.74
C0600-081-1000					1.00	25.40			0.719	18.26	0.552	14.02	116.2	20.35
C0600-081-1250					1.25	31.75			0.885	22.48	0.644	16.36	89.5	15.67
C0600-081-1500					1.50	38.10			1.051	26.70	0.736	18.69	72.8	12.75
C0600-081-1750			1.75	44.45	1.217	30.91	0.828	21.03	61.3	10.73				
C0600-081-2000			2.00	50.80	1.383	35.13	0.920	23.37	53.0	9.28				
C0600-081-2250			2.25	57.15	1.549	39.34	1.012	25.70	46.6	8.16				
C0600-081-2500			2.50	63.50	1.715	43.56	1.104	28.04	41.7	7.30				
C0600-081-2750			2.75	69.85	1.881	47.78	1.196	30.38	37.6	6.58				
C0600-081-3000			3.00	76.20	2.047	51.99	1.288	32.72	34.3	6.01				
C0600-081-3250			3.25	82.55	2.213	56.21	1.380	35.05	31.5	5.52				
C0600-081-3500			3.50	88.90	2.379	60.43	1.472	37.39	29.2	5.11				
C0600-081-3750			3.75	95.25	2.545	64.64	1.564	39.73	27.1	4.75				
C0600-081-4000			4.00	101.60	2.711	68.86	1.656	42.06	25.4	4.45				
C0600-085-0620			0.085	2.16	0.62	15.75	37.62	167.33	0.477	12.12	0.433	11.00	262.5	45.96
C0600-085-0750					0.75	19.05			0.565	14.35	0.484	12.29	203.6	35.65
C0600-085-0880	0.88	22.35			0.654	16.61			0.536	13.61	166.4	29.14		
C0600-085-1000	1.00	25.40			0.736	18.69			0.583	14.81	142.3	24.92		
C0600-085-1250	1.25	31.75			0.906	23.01			0.682	17.32	109.4	19.16		
C0600-085-1500	1.50	38.10			1.076	27.33			0.781	19.84	88.8	15.55		
C0600-085-1750	1.75	44.45	1.247	31.67	0.880	22.35	74.8	13.10						
C0600-085-2000	2.00	50.80	1.417	35.99	0.978	24.84	64.5	11.29						
C0600-085-2250	2.25	57.15	1.588	40.34	1.077	27.36	56.8	9.95						
C0600-085-2500	2.50	63.50	1.758	44.65	1.176	29.87	50.7	8.88						
C0600-085-2750	2.75	69.85	1.928	48.97	1.275	32.39	45.8	8.02						
C0600-085-3000	3.00	76.20	2.099	53.31	1.374	34.90	41.7	7.30						
C0600-085-3250	3.25	82.55	2.269	57.63	1.473	37.41	38.3	6.71						
C0600-085-3500	3.50	88.90	2.439	61.95	1.572	39.93	35.5	6.22						
C0600-085-3750	3.75	95.25	2.610	66.29	1.670	42.42	33.0	5.78						
C0600-085-4000	4.00	101.60	2.780	70.61	1.769	44.93	30.8	5.39						
C0600-092-0750	0.092	2.34	0.75	19.05	46.46	206.65	0.591	15.01	0.524	13.31	291.5	51.04		
C0600-092-0880			0.88	22.35			0.684	17.37	0.581	14.76	237.0	41.50		
C0600-092-1000			1.00	25.40			0.770	19.56	0.633	16.08	202.2	35.41		

†For stainless steel, multiply values by 0.833.

\*When inquiring or ordering, use letter "M" or letter "S" as suffix on catalog numbers to designate music wire or stainless-steel wire, respectively.



# Constant-force Springs



## Stock sizes in stainless steel

Constant-force springs are a special variety of extension spring. They consist of a spiral of strip material with built-in curvature so that each turn of the strip wraps tightly on its inner neighbor. When the strip is extended (deflected) the inherent stress resists the loading force, just as in a common extension spring, but at a nearly constant (zero) rate. The accompanying load/deflection curves illustrate this.

The constant-force spring is well suited to long extensions with no load build-up. In use, the spring is usually mounted with the ID tightly wrapped on a drum and the free end attached to the loading force, such as in a counterbalance application. This relationship can be reversed, however, with the free end mounted stationary and the spring itself providing the working force, as with carbon brushes in electrical apparatus.

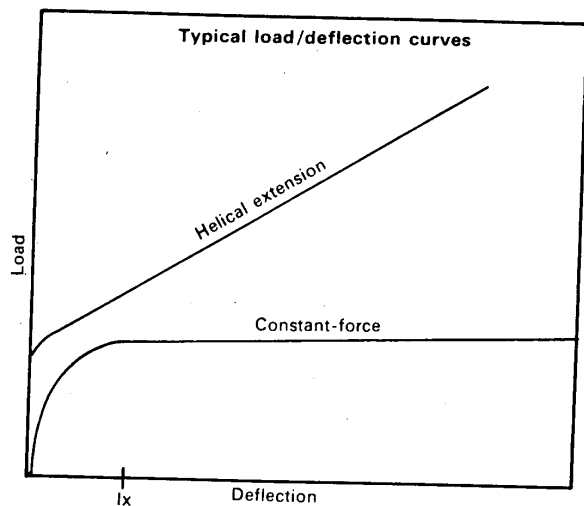
Considerable flexibility is possible with constant-force springs because the load capacity can be multiplied by using two or more strips in tandem, back-to-back, or laminated, as illustrated.

## Material

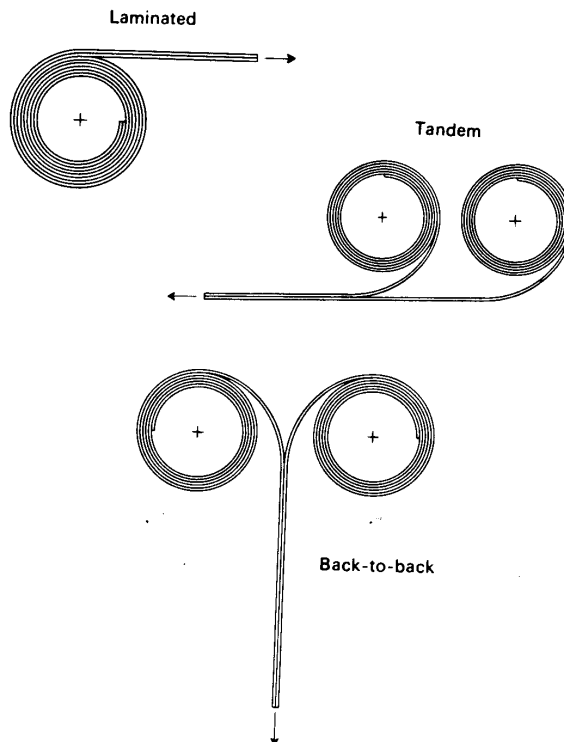
Type 301 stainless steel.

### Note

Be sure to allow at least 1½ coils of material on the drum at full extension. The spring ID will wrap tightly on the drum so that in most applications no fastening method on the drum is required.



## How to multiply constant-force spring load



# THE 1999 FIRST ROBOTICS COMPETITION MANUAL

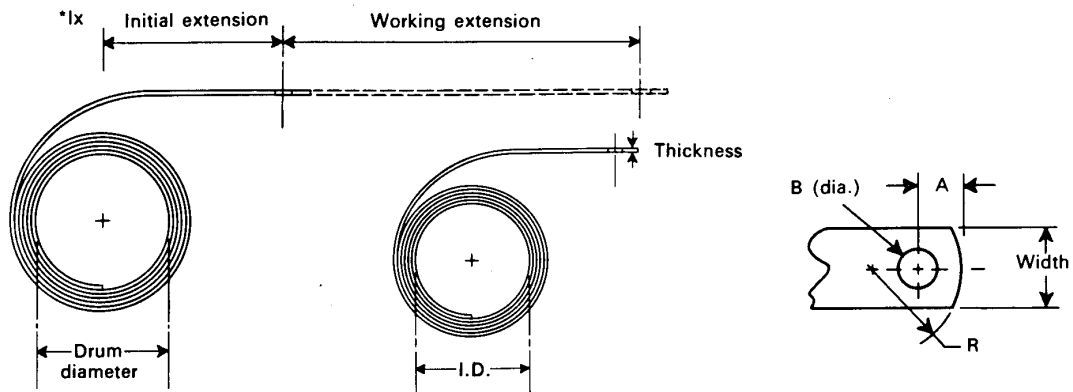
## STOCK CONSTANT-FORCE SPRINGS Stainless Steel



Associated Spring  
Raymond BARNES  
GROUP INC.

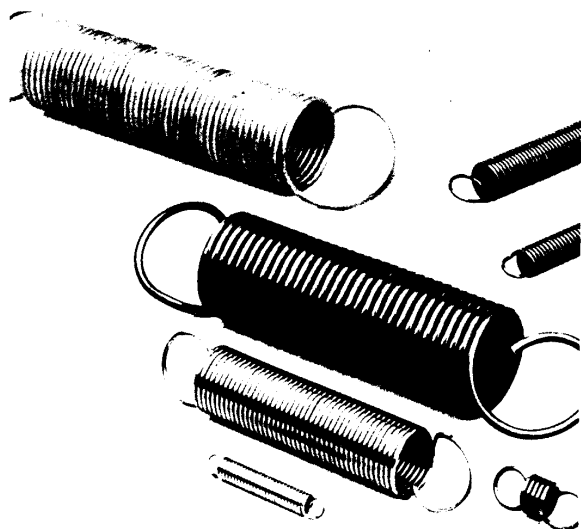
CATALOG NUMBER	Thickness		Width		Length		Initial Extension		Working Ext.		I.D. (Reference)		Drum Diameter		Load ±10%		End Configuration					
																	A		B		R	
	in	mm	in	mm	in	mm	in	mm	in	mm	in	mm	in	mm	lb	N	in	mm	in	mm	in	mm
Fatigue Life 4,000 Cycles																						
CF015-0050	0.004	0.10	0.25	6.35	15	381	0.61	15.49	12	305	0.34	8.64	0.40	10.16	0.50	2.22	3/8	9.5	0.131	3.3	1/2	12.7
CF018-0075	0.005	0.13	0.31	7.87	18	457	0.75	19.05	15	381	0.42	10.67	0.50	12.70	0.75	3.34	3/8	9.5	0.131	3.3	1/2	12.7
CF022-0112	0.006	0.15	0.37	9.40	22	559	0.92	23.37	18	457	0.51	12.95	0.62	15.75	1.12	4.98	3/8	9.5	0.131	3.3	1/2	12.7
CF026-0162	0.007	0.18	0.50	12.70	26	660	1.06	26.92	21	533	0.59	14.99	0.75	19.05	1.62	7.21	3/8	9.5	0.131	3.3	1/2	12.7
CF030-0237	0.008	0.20	0.59	14.99	30	762	1.22	30.99	24	610	0.68	17.27	0.87	22.10	2.37	10.54	3/8	9.5	0.187	4.7	7/8	22.2
CF034-0350	0.010	0.25	0.68	17.27	34	864	1.53	38.86	27	686	0.85	21.59	1.00	25.40	3.50	15.57	3/8	9.5	0.187	4.7	7/8	22.2
CF038-0500	0.012	0.30	0.81	20.57	38	965	1.84	46.74	30	762	1.02	25.91	1.25	31.75	5.00	22.24	3/8	9.5	0.187	4.7	7/8	22.2
CF043-0700	0.014	0.36	1.00	25.40	43	1092	2.14	54.36	33	838	1.19	30.23	1.50	38.10	7.00	31.14	3/8	9.5	0.187	4.7	7/8	22.2

Fatigue Life 40,000 Cycles																						
CF021-0025	0.006	0.15	0.37	9.40	21	533	2.03	51.56	12	305	1.13	28.70	1.36	34.54	0.25	1.11	3/8	9.5	0.131	3.3	1/2	12.7
CF025-0037	0.007	0.18	0.50	12.70	25	635	2.36	59.94	15	381	1.31	33.27	1.58	40.13	0.37	1.65	3/8	9.5	0.131	3.3	1/2	12.7
CF030-0050	0.008	0.20	0.59	14.99	30	762	2.72	69.09	18	457	1.51	38.35	1.81	45.97	0.50	2.22	3/8	9.5	0.187	4.7	7/8	22.2
CF036-0075	0.010	0.25	0.68	17.27	36	914	3.38	85.85	21	533	1.88	47.75	2.26	57.40	0.75	3.34	3/8	9.5	0.187	4.7	7/8	22.2
CF042-0112	0.012	0.30	0.81	20.57	42	1067	4.07	103.40	24	610	2.26	57.40	2.71	68.83	1.12	4.98	3/8	9.5	0.187	4.7	7/8	22.2
CF048-0162	0.014	0.36	1.00	25.40	48	1219	4.74	120.40	27	686	2.63	66.80	3.16	80.26	1.62	7.21	3/8	9.5	0.187	4.7	7/8	22.2



\*Initial extension is the minimum amount of extension needed to operate the spring and achieve a linear rate. (see chart page 77)

# Extension Springs



## Stock sizes in music wire and stainless steel

All SPEC stock helical extension springs have uniform body diameter and are produced with full twist loops the same diameter as the body. They are wound with initial tension; some force is required before the coils are initially separated. As with other Associated Spring stock components, they are capable of wide application for experimental, development, prototype and maintenance work.

## Material

### Music wire

ASTM-A228 or AMS 5112

### Stainless steel

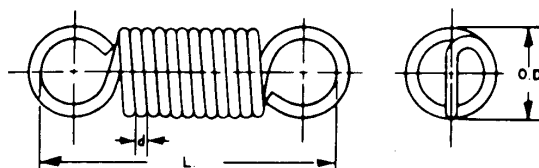
Commercial Type 302, ASTM-A313 or

AMS 5688 spring temper. (chemical & physical only)

No charge for certificate of compliance when requested; certificate of chemical analysis available, see price book.

Music wire will be furnished unless stainless steel is specified. When inquiring or ordering, use letter "M" or letter "S" as suffix on catalog numbers to designate music wire or stainless steel wire, respectively.

Music wire springs are not recommended for applications where the temperature exceeds 250 deg F (121 deg C). Stainless steel springs are not recommended for applications where the temperature exceeds 500 deg F (260 deg C).



## Direction of Helix

Right or left according to machine set-up at time of run.

## Ends

Full twist loop. Special ends on request.

Initial tension T is for reference only; free length dimension L is approximate.

Maximum load P is attained at extended length L<sub>1</sub>.

To determine load P, rate R or initial tension T, for stainless steel, multiply the values given by 0.833. To determine load P\* at any extension other than L<sub>1</sub>, multiply the distance in inches that the spring will be extended from the free length L, by the spring rate R and add the initial tension T.

## Finishes

Standard finish is that of the normal wire. Shot-peened and plated finishes furnished on request. Allow additional time for special finishes.

## Tolerances

O.D. (English)	O.D. (Metric)
0.063 to 0.119 in ± 0.003 in	1.60 to 3.02 mm ± 0.08 mm
0.120 to 0.240 in ± 0.005 in	3.05 to 6.10 mm ± 0.13 mm
0.241 to 0.500 in ± 0.008 in	6.12 to 12.70 mm ± 0.20 mm
0.501 to 1.000 in ± 0.015 in	12.73 to 25.40 mm ± 0.38 mm
1.001 to 1.225 in ± 0.020 in	25.43 to 31.12 mm ± 0.51 mm
1.226 to 1.460 in ± 0.030 in	31.14 to 37.08 mm ± 0.76 mm
1.461 to 2.000 in ± 0.040 in	37.11 to 50.80 mm ± 1.02 mm

Load, P ± 10%  
Spring Rate, R ± 10%  
Position of Ends ± 22 deg

$$*P = (Lx - L) \times R + T$$

Lx = Desired Load Length

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# THE 1999 FIRST ROBOTICS COMPETITION MANUAL

## STOCK EXTENSION SPRINGS Music Wire and Stainless Steel



CATALOG NUMBER*	Outside Diameter		Wire Diameter		Free Length L, Approx.		Load, P at L <sub>1</sub>		Initial Tension, T**		Ext. L <sub>1</sub>		Spring Rate, R	
	in	mm	in	mm	in	mm	lb†	N†	lb†	N†	in	mm	lb/in†	N/mm†
E0420-055-1500	0.420	10.67	0.055	1.40	1.50	38.10	15.80	70.28	1.40	6.23	2.24	56.90	19.5	3.41
E0420-055-1750					1.75	44.45					2.73	69.34	14.7	2.57
E0420-055-2000					2.00	50.80					3.22	81.79	11.8	2.07
E0420-055-2250					2.25	57.15					3.71	94.23	9.8	1.716
E0420-055-2500					2.50	63.50					4.21	106.93	8.4	1.471
E0420-055-2750					2.75	69.85					4.70	119.38	7.4	1.296
E0420-055-3000					3.00	76.20					5.19	131.83	6.6	1.156
E0500-034-1250	0.500	12.70	0.034	0.86	1.25	31.75	3.49	15.52	0.31	1.38	2.56	65.02	2.4	0.420
E0500-034-1370					1.37	34.80					3.27	83.06	1.7	0.298
E0500-034-1500					1.50	38.10					4.04	102.62	1.3	0.228
E0500-034-1750					1.75	44.45					5.52	140.21	0.8	0.140
E0500-034-2000					2.00	50.80					7.00	177.80	0.6	0.105
E0500-034-2250					2.25	57.15					8.48	215.39	0.5	0.088
E0500-037-1250					1.25	31.75					2.65	67.31	2.8	0.490
E0500-037-1370					1.37	34.80					3.20	81.28	2.1	0.368
E0500-037-1500					1.50	38.10					3.81	96.77	1.7	0.298
E0500-037-1750					1.75	44.45					4.98	126.49	1.2	0.210
E0500-037-2000					2.00	50.80					6.12	155.45	1.0	0.175
E0500-037-2250					2.25	57.15					7.37	187.20	0.8	0.140
E0500-037-2500			0.037	0.94	2.50	63.50	4.40	19.57	0.40	1.78	8.54	216.92	0.7	0.123
E0500-037-2750					2.75	69.85					9.82	249.43	0.6	0.105
E0500-037-3000					3.00	76.20					11.10	281.94	0.5	0.088
E0500-037-3500					3.50	88.90					13.59	345.19	0.4	0.070
E0500-037-4000					4.00	101.60					16.08	408.43	0.3	0.053
E0500-037-4500					4.50	114.30					18.57	471.68	0.3	0.053
E0500-037-5000					5.00	127.00					21.06	534.92	0.2	0.035
E0500-041-1250					1.25	31.75					2.34	59.44	4.8	0.841
E0500-041-1370					1.37	34.80					2.83	71.88	3.6	0.630
E0500-041-1500					1.50	38.10					3.32	84.33	2.9	0.508
E0500-041-1750					1.75	44.45					4.29	108.97	2.0	0.350
E0500-041-2000					2.00	50.80					5.33	135.38	1.5	0.263
E0500-041-2250					2.25	57.15					6.30	160.02	1.3	0.228
E0500-041-2500			0.041	1.04	2.50	63.50	5.80	25.80	0.50	2.22	7.31	185.67	1.1	0.193
E0500-041-2750					2.75	69.85					8.34	211.84	1.0	0.175
E0500-041-3000					3.00	76.20					9.38	238.25	0.8	0.140
E0500-041-3500					3.50	88.90					11.32	287.53	0.7	0.123
E0500-041-4000					4.00	101.60					13.34	338.84	0.6	0.105
E0500-041-4500					4.50	114.30					15.41	391.41	0.5	0.088
E0500-041-5000					5.00	127.00					17.43	442.72	0.4	0.070
E0500-045-1250					1.25	31.75					2.00	50.80	9.3	1.629
E0500-045-1370					1.37	34.80					2.58	65.53	5.6	0.981
E0500-045-1500					1.50	38.10					2.94	74.68	4.6	0.806
E0500-045-1750					1.75	44.45					3.79	96.27	3.3	0.578
E0500-045-2000					2.00	50.80					4.61	117.09	2.6	0.455
E0500-045-2250					2.25	57.15					5.49	139.45	2.1	0.368
E0500-045-2500			0.045	1.14	2.50	63.50	7.50	33.36	0.70	3.11	6.36	161.54	1.8	0.315
E0500-045-2750					2.75	69.85					7.23	183.64	1.6	0.280
E0500-045-3000					3.00	76.20					8.10	205.74	1.4	0.245
E0500-045-3500					3.50	88.90					9.64	244.86	1.1	0.193
E0500-045-4000					4.00	101.60					11.39	289.31	0.9	0.158
E0500-045-4500					4.50	114.30					13.08	332.23	0.8	0.140
E0500-045-5000					5.00	127.00					14.78	375.41	0.7	0.123
E0500-049-1250					1.25	31.75					1.88	47.75	14.0	2.45
E0500-049-1370					1.37	34.80					2.25	57.15	10.1	1.769
E0500-049-1500					1.50	38.10					2.64	67.06	7.8	1.366
E0500-049-1750					1.75	44.45					3.39	86.11	5.4	0.946
E0500-049-2000					2.00	50.80					4.14	105.16	4.2	0.736
E0500-049-2250			0.049	1.24	2.25	57.15	9.75	43.37	0.88	3.91	4.89	124.21	3.4	0.595
E0500-049-2500					2.50	63.50					5.64	143.26	2.8	0.490
E0500-049-2750					2.75	69.85					6.39	162.31	2.4	0.420
E0500-049-3000					3.00	76.20					7.14	181.36	2.1	0.368
E0500-049-3500					3.50	88.90					8.64	219.46	1.7	0.298
E0500-049-4000					4.00	101.60					10.15	257.81	1.4	0.245
E0500-049-4500					4.50	114.30					11.67	296.42	1.2	0.210
E0500-049-5000					5.00	127.00					13.15	334.01	1.1	0.193

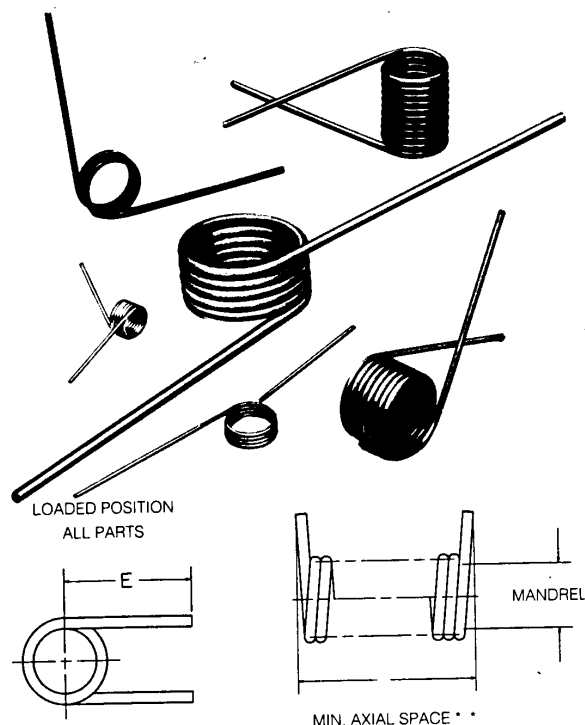
†For stainless steel, multiply values by 0.833.

\*When inquiring or ordering, use letter "M" or letter "S" as suffix on catalog numbers to designate music wire or stainless-steel wire, respectively.

\*\*Initial tension is for reference only and may vary.



# Torsion Springs



## Material

Stainless steel

Commercial Type 302 ASTM-A313 or  
AMS 5688 (chemical & physical only)

No charge for certificate of compliance when requested;  
certificate of chemical analysis available, see price book.  
**See Page 77 for music wire torsion springs.**

## Direction of Helix

Must be specified by suffix to catalog number. Use L for left-hand wound, R for right-hand wound.

## Ends

Straight torsion ends are standard.

## Finish

Plain finish is standard. Allow additional time for special finishes.

## Tolerances

Torque  $\pm 10\%$   
O.D.  $\pm 5\%$

## Stock sizes in stainless steel

Associated Spring torsion springs are widely used to store and release energy of rotation or to maintain a pressure over a short distance. Our stock selection includes torsion springs with four end positions, as shown in the drawings on this page.

SPEC torsion springs are normally used over a supporting mandrel or arbor. Suggested mandrel sizes allow about 10% clearance at the deflections listed. If greater deflections are used, the arbor size should be reduced. Sufficient room (minimum axial space) must be provided in the assembly for the spring to function properly. The minimum axial space does not refer to the length of the coils.

SPEC torsion springs should be used in the direction that winds the coils. In the unwinding direction the maximum load is lower because of residual stresses.

Torque values listed are recommended maximum torques. These values can be increased about 20% for static conditions with only slight setting.

For inspection purposes the load should be applied at  $\frac{1}{2}$  leg length (E). Using other lengths appreciably alter the active length of wire and affect the test results.

The torque values listed can be translated to direct load

by use of the formula  $P = \frac{M}{E_n}$  where P is the load applied

at the new leg length  $E_n$ . Example: For part T012-090-055,

what is the load when  $E_n = 0.187$ ?  $P = \frac{M}{E_n} = \frac{0.047}{0.187} = 0.25 \text{ lb.}$

The torque values listed will be attained at the deflections listed. Torque values at intermediate deflections can be computed by direct proration. Example: For part T030-180-250, the torque at 90 deg deflection is 0.312 in-lb.

**Figures show springs wound left-hand**

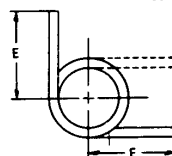


Fig. 1  
90° Deflection

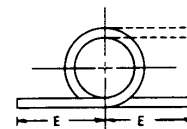


Fig. 2  
180° Deflection

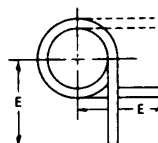


Fig. 3  
270° Deflection

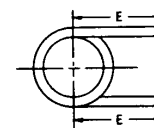


Fig. 4  
360° Deflection

Dotted lines represent final loaded position.

# THE 1999 FIRST ROBOTICS COMPETITION MANUAL

## STOCK TORSION SPRINGS Stainless Steel



Associated Spring  
Raymond BARNES  
GROUP INC.

CATALOG NUMBER*	Wire Diameter		Outside Diameter		Pos. of Ends, Fig.	Def., Deg.	Torque M		Test Point ½ E		Suggested Mandrel Size		E		Min. Axial Space**	
	in	mm	in	mm			in-lb	N-mm	in	mm	in	mm	in	mm	in	mm
T032-090-172	0.032	0.81	0.288	7.32	1	90	0.820	92.7	0.500	12.70	0.172	4.36	1.000	25.40	0.152	3.86
T032-180-156			0.270	6.86	2	180			0.500	12.70	0.156	3.96	1.000	25.40	0.272	6.91
T032-270-156			0.264	6.71	3	270			0.500	12.70	0.156	3.96	1.000	25.40	0.382	9.70
T032-180-218			0.366	9.30	2	180			0.500	12.70	0.218	5.54	1.000	25.40	0.208	5.28
T032-270-218			0.354	8.99	3	270			0.500	12.70	0.218	5.54	1.000	25.40	0.296	7.52
T032-360-234			0.382	9.70	4	360			0.500	12.70	0.234	5.95	1.000	25.40	0.352	8.94
T035-090-187	0.035	0.89	0.315	8.00	1	90	1.000	113.0	0.625	15.88	0.187	4.75	1.250	31.75	0.135	3.43
T035-180-187			0.303	7.70	2	180			0.625	15.88	0.187	4.75	1.250	31.75	0.290	7.37
T035-270-187			0.311	7.90	3	270			0.625	15.88	0.187	4.75	1.250	31.75	0.442	11.23
T035-180-281			0.450	11.43	2	180			0.625	15.88	0.281	7.14	1.250	31.75	0.212	5.38
T035-270-281			0.435	11.05	3	270			0.625	15.88	0.281	7.14	1.250	31.75	0.328	8.33
T035-360-312			0.471	11.96	4	360			0.625	15.88	0.312	7.92	1.250	31.75	0.405	10.29
T038-090-234	0.038	0.97	0.386	9.80	1	90	1.190	134.5	0.625	15.88	0.234	5.94	1.250	31.75	0.180	4.57
T038-180-218			0.368	9.35	2	180			0.625	15.88	0.218	5.54	1.250	31.75	0.323	8.20
T038-270-218			0.353	8.97	3	270			0.625	15.88	0.218	5.54	1.250	31.75	0.465	11.81
T038-180-312			0.487	12.37	2	180			0.625	15.88	0.318	8.08	1.250	31.75	0.247	6.27
T038-270-312			0.477	12.12	3	270			0.625	15.88	0.312	7.92	1.250	31.75	0.352	8.94
T038-360-328			0.514	13.06	4	360			0.625	15.88	0.328	8.33	1.250	31.75	0.418	10.62
T040-090-187	0.040	1.02	0.309	7.85	1	90	1.375	155.4	0.625	15.88	0.187	4.75	1.250	31.75	0.198	5.03
T040-180-218			0.348	8.84	2	180			0.625	15.88	0.218	5.54	1.250	31.75	0.374	9.50
T040-270-218			0.358	9.09	3	270			0.625	15.88	0.218	5.54	1.250	31.75	0.550	13.97
T040-180-343			0.518	13.16	2	180			1.000	25.40	0.343	8.71	2.000	50.80	0.242	6.15
T040-270-343			0.511	12.98	3	270			1.000	25.40	0.343	8.71	2.000	50.80	0.374	9.50
T040-360-343			0.507	12.88	4	360			1.000	25.40	0.343	8.71	2.000	50.80	0.508	12.90
T045-090-203	0.045	1.14	0.357	9.07	1	90	2.000	226.	0.625	15.88	0.203	5.16	1.250	31.75	0.259	6.58
T045-180-218			0.377	9.58	2	180			0.625	15.88	0.218	5.54	1.250	31.75	0.427	10.85
T045-270-234			0.382	9.70	3	270			0.625	15.88	0.234	5.94	1.250	31.75	0.595	15.11
T045-180-359			0.575	14.61	2	180			1.000	25.40	0.359	9.12	2.000	50.80	0.293	7.44
T045-270-359			0.556	14.12	3	270			1.000	25.40	0.359	9.12	2.000	50.80	0.415	10.54
T045-360-359			0.549	13.94	4	360			1.000	25.40	0.359	9.12	2.000	50.80	0.540	13.72
T048-090-218	0.048	1.22	0.375	9.53	1	90	2.500	282.	0.625	15.88	0.218	5.54	1.250	31.75	0.238	6.05
T048-180-250			0.404	10.26	2	180			0.625	15.88	0.250	6.35	1.250	31.75	0.450	11.43
T048-270-250			0.416	10.57	3	270			0.625	15.88	0.250	6.35	1.250	31.75	0.660	16.76
T048-180-406			0.618	15.70	2	180			1.000	25.40	0.406	10.31	2.000	50.80	0.292	7.42
T048-270-406			0.600	15.24	3	270			1.000	25.40	0.406	10.31	2.000	50.80	0.450	11.43
T048-360-406			0.594	15.09	4	360			1.000	25.40	0.406	10.31	2.000	50.80	0.610	15.49
T051-090-234	0.051	1.30	0.408	10.36	1	90	2.900	328.	1.000	25.40	0.234	5.94	2.000	50.80	0.293	7.44
T051-180-250			0.430	10.92	2	180			1.000	25.40	0.250	6.35	2.000	50.80	0.485	12.32
T051-270-266			0.439	11.15	3	270			1.000	25.40	0.266	6.76	2.000	50.80	0.675	17.15
T051-180-344			0.556	14.12	2	180			1.000	25.40	0.344	8.74	2.000	50.80	0.382	9.70
T051-270-359			0.571	14.50	3	270			1.000	25.40	0.359	9.12	2.000	50.80	0.522	13.26
T051-360-406			0.628	15.95	4	360			1.000	25.40	0.406	10.31	2.000	50.80	0.615	15.62
T054-090-296	0.054	1.37	0.484	12.29	1	90	3.275	370.	1.000	25.40	0.296	7.52	2.000	50.80	0.310	7.87
T054-180-312			0.509	12.93	2	180			1.000	25.40	0.312	7.92	2.000	50.80	0.512	13.00
T054-270-312			0.514	13.06	3	270			1.000	25.40	0.312	7.92	2.000	50.80	0.715	18.16
T054-180-421			0.654	16.61	2	180			1.000	25.40	0.421	10.69	2.000	50.80	0.405	10.26
T054-270-437			0.664	16.81	3	270			1.000	25.40	0.437	11.10	2.000	50.80	0.555	14.10
T054-360-453			0.694	16.61	4	360			1.000	25.40	0.453	11.51	2.000	50.80	0.705	17.91
T059-090-296	0.059	1.50	0.499	12.67	1	90	4.200	475.	1.000	25.40	0.296	7.52	2.000	50.80	0.340	8.64
T059-180-328			0.526	13.36	2	180			1.000	25.40	0.328	8.33	2.000	50.80	0.560	14.22
T059-270-328			0.537	13.64	3	270			1.000	25.40	0.328	8.33	2.000	50.80	0.785	19.94
T059-180-437			0.681	17.30	2	180			1.000	25.40	0.437	11.10	2.000	50.80	0.445	11.30
T059-270-453			0.699	17.75	3	270			1.000	25.40	0.453	11.51	2.000	50.80	0.605	15.37
T059-360-459			0.709	18.01	4	360			1.000	25.40	0.459	11.66	2.000	50.80	0.770	19.56
T063-090-343	0.063	1.60	0.560	14.22	1	90	5.150	582.	1.000	25.40	0.343	8.71	2.000	50.80	0.362	9.19
T063-180-359			0.591	15.01	2	180			1.000	25.40	0.359	9.12	2.000	50.80	0.600	15.24
T063-270-375			0.600	15.24	3	270			1.000	25.40	0.375	9.53	2.000	50.80	0.835	21.21
T063-180-500			0.767	19.48	2	180			1.000	25.40	0.500	12.70	2.000	50.80	0.475	12.07
T063-270-516			0.784	19.91	3	270			1.000	25.40	0.516	13.11	2.000	50.80	0.645	16.38
T063-360-516			0.798	20.27	4	360			1.000	25.40	0.516	13.11	2.000	50.80	0.820	20.83
T070-090-359	0.070	1.78	0.593	15.06	1	90	7.000	791.	1.000	25.40	0.359	9.12	2.000	50.80	0.400	10.16
T070-180-390			0.625	15.88	2	180			1.000	25.40	0.390	9.91	2.000	50.80	0.665	16.89
T070-270-390			0.639	16.23	3	270			1.000	25.40	0.390	9.91	2.000	50.80	0.930	23.62
T070-180-515			0.810	20.57	2	180			1.000	25.40	0.515	13.08	2.000	50.80	0.525	13.34
T070-270-531			0.826	20.98	3	270			1.000	25.40	0.531	13.49	2.000	50.80	0.717	18.21
T070-360-546			0.843	21.41	4	360			1.000	25.40	0.546	13.87	2.000	50.80	0.910	23.11

\*Indicate direction of helix desired by suffix to catalog number — L for left hand wound, R for right hand wound.  
\*\*Space needed on application to allow for operation of the spring. This dimension does not refer to the length of the coils.

# THE 1999 FIRST ROBOTICS COMPETITION MANUAL

**BEI** SYSTRON DONNER INERTIAL DIVISION  
SENSORS & SYSTEMS COMPANY



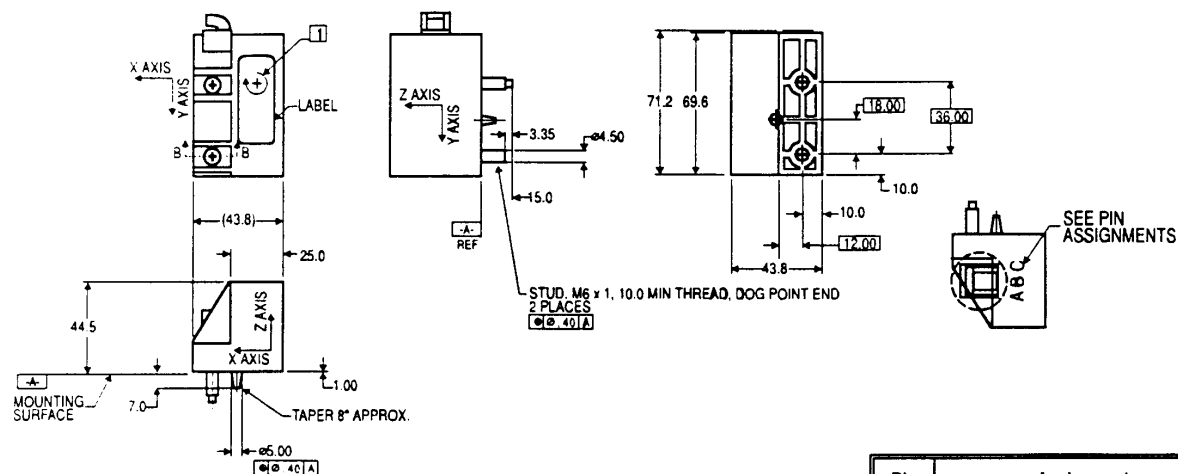
## GyroChip®

Solid State Gyroscope

## FIRST Project

AQRS-00064-109

PARAMETER	SUMMARY SPECIFICATION
<b>POWER REQUIREMENTS</b>	
Operating Voltage	+5 VDC $\pm 0.25$ VDC
Operating Current	20 mA (max.)
<b>PERFORMANCE</b> (typical for 5 Volt input)	
Range*	$\pm 64^\circ/\text{sec}$
Scale Factor*	
Full Range Output	+0.25 to +4.75 VDC
Nominal	35.16 mV/ $^\circ/\text{sec}$
Bias*	
Bias at Ambient	+2.50 VDC $\pm 0.5$
Bandwidth (90°)	>50 Hz
* Note: Output is ratiometric to supply voltage.	
<b>ENVIRONMENTS</b>	
Operating Temperature	70°F to 90°F
Storage Temperature	-40°F to +185°F
Vibration Operating	1.5 g RMS, 20 to 2,000 Hz
<b>WEIGHT</b>	125 grams max.



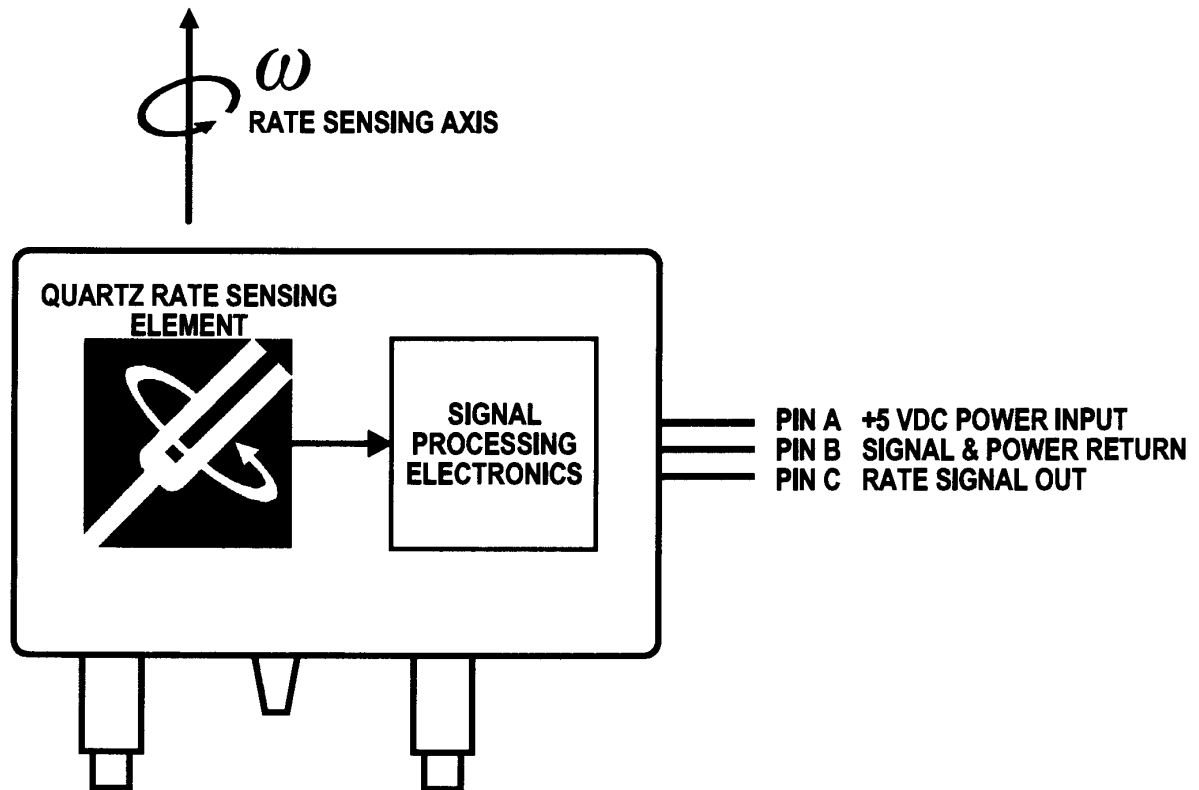
**Not Supplied:**  
Mating Connector Kit (Pioneer Standard)  
3 WAY Female – P/N 12064758 (1 ea.)  
Terminal Female – P/N 12047767 (3 ea.)

### NOTES:

1. ANGULAR RATE APPLIED AS SHOWN SHALL PRODUCE A MORE POSITIVE OUTPUT.
2. DIMENSIONS SHOWN ARE IN MILLIMETERS

Pin	Assignment
A	+5 VDC Input
B	Common
C	Rate Out (1 Kohn output impedance)

Syston Donner Inertial Division • 2700 Syston Drive • Concord, California 94518 • Toll Free: (800) 227-1625  
Sales: (925) 671-6601 • Customer Service: (925) 671-6499 • FAX: (925) 671-6647  
European Business Office (Ashford, England): 44 1303 812778 • FAX: 44 1303 812708



## Quartz Rate Sensor "GyroChip®"

**NOT SUPPLIED:**  
**Mating Connector Kit (Pioneer Standard)**  
3 Way Female - P/N 12064758 (1 ea.)  
Terminal Female - P/N 12047767 (3 ea.)

### NOTES:

- Rate Sensor Output is ratiometric to input power line voltage over the range of +4.75 to +5.25 VDC.
- Full scale factor rate range is  $\pm 64^\circ/\text{sec}$ .
- Output signal is symmetrical about a +2.5 VDC (nominal) bias.
- Output Impedance is  $1\text{K}\Omega$  or less.

12/98:FIRSTOD CDR.JSAS

**BEI** SYSTRON DONNER INERTIAL DIVISION  
SENSORS & SYSTEMS COMPANY

# A Quartz Rotational Rate Sensor

Based on inertial-sensing principles, the quartz rate sensor provides a simple, reliable measurement of rotational velocity.

The use of a vibrating element to measure rotational velocity by employing the Coriolis principle is a concept that has been around for more than 50 years. In fact, the idea developed long ago out of the observation that a certain species of fly uses a pair of vibrating antennae to stabilize its flight. This sensing technique has been given a practical embodiment: the quartz rate sensor (QRS).

## THEORY OF OPERATION

To understand how the QRS works requires familiarity with the Coriolis principle. Simply stated, this means that a linear motion within a rotating framework will have some component of velocity that is perpendicular to that linear motion.

The handiest example of the Coriolis effect is that exhibited by wind patterns on Earth. Convection cells in the atmosphere set up a wind flow from the poles toward the equator (with a north-south orientation). The Earth's rotation, however, causes these linear flows to develop a sideways (orthogonal) component of motion. This "bends" the wind from a north-south to an east-west direction. It is the Coriolis effect that creates the east-west "trade winds," and which is responsible for the spirals of clouds observed in satellite photos.

Now let's apply this principle to our rotation sensor. In Figure 1 you can see that the QRS is essentially divided into

two sections: drive and pickup.

The drive portion looks and acts exactly like a simple tuning fork. Because the drive tines are constructed of crystalline quartz, it is possible to electrically "ring" this tuning fork. Each fork tine has a mass and an instantaneous radial velocity that changes sinusoidally as the tine moves back and forth. As long as the fork's base is stationary, the momenta of the two tines exactly cancel each other and there is no energy transfer from the tines to the base. In fact, it takes only  $\sim 6 \mu\text{W}$  of power to keep the fork ringing.

As soon as the tuning fork is rotated around its axis of symmetry, however, the Coriolis principle exerts a profound influence on the behavior of this mechanism.

By convention (the "right-hand rule"), the rotational vector  $\omega_i$  is described by an arrow that is aligned with the axis of rotation. The instantaneous radial velocity of each of the tines will, through the Coriolis effect, generate a vector cross-product with this rotation vector.

The net effect is that each tine will generate a force perpendicular to the instantaneous radial velocity of each of the other tines:

$$F = 2m\omega_i \cdot V_r \quad (1)$$

where:

$$\begin{aligned} m &= \text{tine mass} \\ \omega_i &= \text{rotation rate} \\ V_r &= \text{radial velocity} \end{aligned}$$

Note that this force is directly proportional to the rotation rate, and since the radial velocity of the tines is sinusoidal, the resultant force on each tine is also sinusoidal. Because the radial velocities of the two tines are equal and opposite,

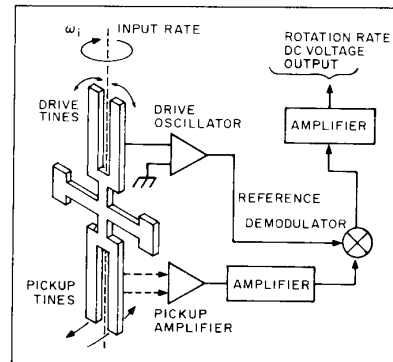


Figure 1. An oscillating tuning fork senses rotational velocity by using the Coriolis force to translate the linear motion of the tines into an oscillating torque. This torque value is demodulated at the oscillation frequency to generate a DC voltage proportional to the rotation rate input.

the Coriolis forces are equal and opposite, producing an oscillating torque at the base of the drive tine fork that is proportional to the input angular rate.

The pickup portion of the QRS now comes into play. The sinusoidal torque variation causes the pickup tines to begin moving tangentially to the rotation and at the same frequency as the drive vibration. Since the forces causing the pickup tines to move are directly proportional to the rotation rate, if there is no rotation the pickup tines will not move. The QRS can therefore truly detect a zero rotation input.

Once the pickup tines are in motion, it is a simple matter to amplify the pickup signal and then demodulate it using the drive frequency as a reference. One additional stage of amplification allows for some signal shaping and produces a DC signal output that is directly propor-

Scott D. Orlosky and Harold D. Morris,  
Syston Donner, a BEI Electronics  
Company

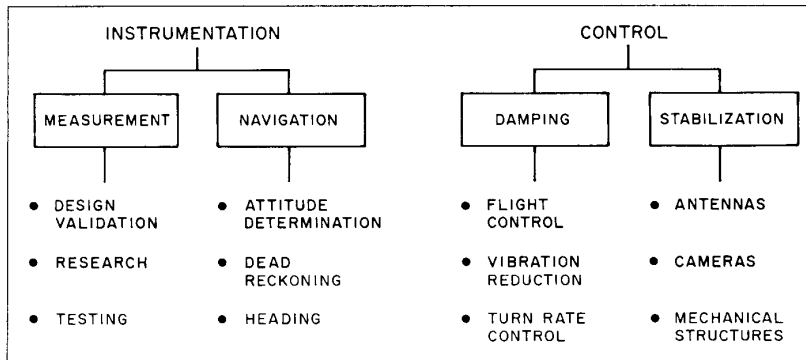


Figure 2. A variety of instrumentation and control applications can benefit from rotational velocity as a means of improving designs, adding navigational capability to autonomous vehicles, and damping out unwanted motions of control surfaces or gimbaled platforms.

tional to the input angular rate. All of the electronics are fairly simple, and can be contained within the same package as the sensing element.

## CONSTRUCTION

The QRS is fabricated from a wafer of single-crystal, synthetically grown quartz. The material's piezoelectric properties are particularly stable over temperature and time. Quartz exhibits a high modulus of elasticity and therefore can be made to ring very precisely with a high  $Q$  (quality factor). In addition, quartz can be worked by using conventional wet chemical etch production techniques similar to those favored by the semiconductor industry for producing chips.

## APPLICATIONS

Until recently, the most common rotation sensors based on the principles of inertial mechanics were spring-restrained spinning-wheel gyroscopes. These tend to be large and heavy, and to consume large quantities of power. They also tend to wear out after only a few thousand hours of operation and so cannot be used continuously for long periods of time. Their use has been restricted to highly specialized applications such as in military aircraft and missiles, where the short mission times and availability of maintenance personnel made their use practical. By contrast, QRS technology, with its MTBF > 100,000 hours and the low cost of ownership, is attractive to industrial and commercial customers as well. QRS applications fall into two broad categories: open-loop, or instrumentation applications; and closed-loop, or control

applications (see Figure 2).

## INSTRUMENTATION

These applications involve either instrumenting a structure for purposes of determining its rates of rotational motion (measurement), or processing that information in real time to generate information about orientation (navigation). Typical examples of rotational velocity measurement include instrumenting vehicles for crash studies, determining dynamics of specific platforms (e.g., boats, trains, robots, or even human beings), and environmental measurements such as earthquakes and wave motions.

**Measurement.** One key element in measurement system design is to determine the peak rotational velocities involved to ensure that an instrument with the proper range is used. If the selected range of the QRS is too low, the output will be clipped and valuable information will be lost.

A fairly straightforward way to determine the correct range requirement is to establish two parameters: the frequency of movement of the structure to be instrumented; and the peak angular displacement of that movement. Let's assume that we want to determine the dynamics of a vehicle's body roll while it takes a turn. The body roll motion can be described as:

$$\theta = A \cdot \sin(2\pi \cdot F_n \cdot t) \text{ in degrees} \quad (2)$$

where:

$A$  = amplitude of movement  
 $F_n$  = frequency of movement

The parameter of interest for measur-

ing angular velocity is the change in angular position with time, or  $(d\theta/dt)$ . Taking the derivative of the above equation:

$$(d\theta/dt) = A \cdot 2\pi \cdot F_n \cdot \cos(2\pi \cdot F_n \cdot t) \quad (3)$$

Let's assume that the natural frequency of the vehicle suspension system is 6 Hz, and the peak body roll is  $10^\circ$ . By substituting these into Equation 3:

$$\begin{aligned} (d\theta/dt) &= 10 \cdot 2\pi \cdot 6 \cdot \cos(2\pi \cdot 6 \cdot t) \\ &= 377 \cdot \cos(37.7 \cdot t)^\circ/\text{s} \end{aligned} \quad (4)$$

Since the cosine term has a maximum value of 1, the peak rotational velocity is  $377^\circ/\text{s}$ . So even a seemingly benign environment, a  $10^\circ$  roll at 6 Hz, generates fairly high peak rotational velocities.

**Navigation.** Navigation applications are becoming increasingly interesting for the QRS, especially in light of the availability of GPS receivers at a reasonable cost. In principle, by reading the output from the rotation sensor (rotational velocity) and integrating this output over time, it is possible to determine the sensor's angular displacement. A QRS can be used for sensing vehicle yaw as part of a navigation package (see Figure 3).

## SYSTEM COMPONENTS

**Anti-Aliasing Filter.** Because a computer interface requires the use of an analog-to-digital (A/D) converter, the output from the QRS becomes part of a sampled data stream. In order to prevent aliasing of the output, a filter must be used with the corner frequency usually set at  $1/4$  to  $1/2$  of the sampling frequency.

**A/D Converter.** The A/D conversion should be carried out immediately after anti-aliasing since this puts the converter close to the QRS and reduces the overall noise of the system, yielding the most stable results. A 12-bit converter is generally adequate. The sample frequency should be appropriate for the system, but typical values range from 100 Hz to 1000 Hz.

**Bandpass Filter.** This filter is tailored to the specific application. When the sensor is used as part of a head-mounted display for a virtual reality application, for example, it is not necessary to track very small, high-frequency head movements because they may simply be part

of the normal jostling associated with interactive game playing. Only larger, definite head swings need attention.

Similarly, low-frequency variations in the QRS output, which are usually associated with changes in environmental temperatures or warm-up, are not meaningful tracking information and should be rejected.

These two scenarios determine the lower and upper ranges of the bandpass filter. A reasonable starting point would be to choose upper and lower corner frequencies of 0.1 Hz and 10 Hz.

**Integrator.** This is where the angular velocity information is turned into angular position. Since the initial conditions are indeterminate at start-up, it is recommended that a reset capability be included. This allows you to initialize the integrator to zero or some known position at startup.

The portion of the platform that is to be measured must usually be held very steady during startup so that the initial conditions represent as closely as possible a true "zero input" state. Any residual error at startup will cause the apparent output from the integrator to drift.

One method to reduce the startup error is to average the input to the integrator for a few seconds during the initialization sequence, and then subtract this average value to establish the zero point.

As a practical matter, it is virtually impossible to measure the "pure" rotational velocity without introducing or reading some error at the same time. This accumulation of errors means that over time, the true angular position and the calculated angular position will diverge. The sensor output may not be drifting, but the apparent calculated angle is.

The rate of this divergence is determined by a variety of factors including: how well the initial conditions are established; the accuracy of the alignment of the sensor to the true axis of rotation; the quantization errors of the signal (if it has been digitized); and the stability of the environment in which the measurement is being done.

For most practical applications, therefore, the QRS is used only for short-term navigation. In order to prevent these incremental errors from growing too large, the common practice is to periodically update, or correct, the calculated angle

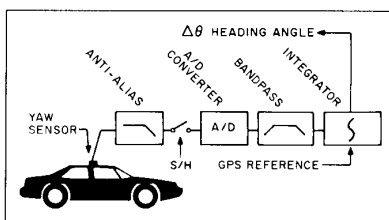


Figure 3. By combining the quartz rotation sensor (QRS) with a fixed reference such as a GPS receiver, a complete navigation system can be created for an automobile. Attention to signal processing design as well as to blending the GPS reference signal produces a system that can cope with extended GPS blackouts.

through the use of a fixed, external reference as shown in Figure 3.

The reference selected will depend on the situation; examples include a GPS signal, a corner-cube with optical line-of-sight, or an encoded magnetic signal. In fact, the combination of dead reckoning between fixed reference updates is a nearly ideal means of navigation through a variety of dynamic environments.

This method has been used for autonomous delivery robots in hospitals, automated forklifts in warehouses, and emergency vehicles deployed in urban environments.

## CONTROL

To employ the QRS in control applications requires an understanding of how it works as part of a system. The typical system model takes into account the magnitude and phase relationships of the sensor response.

**Damping.** The ability to accurately measure rotational velocity opens up new possibilities for control of structures. One of the most useful types of

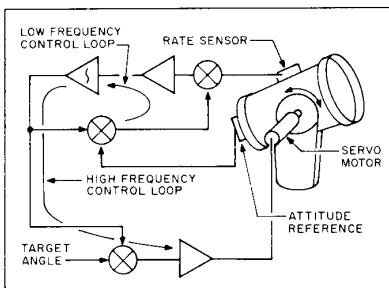


Figure 4. As part of an attitude control system for a mobile telescope, the QRS can be combined with a simple tilt sensor to provide both absolute pointing accuracy as well as stability. Rapid motions are compensated for in the high-frequency control loop, while the low-frequency control loop provides a vertical reference to gravity.

control applications is to damp out the resonant behavior of mechanical systems. Very few mechanical systems produce pure linear motion—most machines have parts that rotate or pivot. Aircraft, land vehicles, and ships are governed by means of roll, pitch, and/or yaw controls. By monitoring and controlling these motions it is possible to provide active roll damping on ships, remove "Dutch roll" from aircraft flight, reduce body roll on a car as it takes a turn, or damp out end-effector shake in an industrial robot.

**Stabilization.** This is a special instance of closed-loop control—stabilization—in which the item being controlled is intended to remain stationary even during movement of the platform to which it is attached. It is important that the QRS be tightly coupled mechanically to the object to be controlled, usually a camera or an antenna on a multi-axis gimbal. This gimbal mechanism must have no mechanical resonances in the bandwidth of the servo-control loop.

The system designer must take into account the transfer function of the system servo-loop and ensure enough phase margin to prevent oscillation. Because it is often necessary to independently move the camera or antenna, a commandable DC offset must be included in the control loop to allow an operator to rotate and point the camera in the gimbal. This method has been used successfully to stabilize antennas aboard ships and land vehicles, as well as cameras aboard helicopters and survey airplanes.

An example of such an application is shown in Figure 4. Here, the QRS is used as part of a servo-control loop to provide an absolute pointing angle in attitude as well as image stability for a mobile telescope.

For simplicity it is assumed that the telescope is mounted on a platform that can rotate only in attitude, and that the control mechanism is therefore an attitude control system only. The principle described can be applied to the other axes of rotation.

Refer first to the high-frequency control loop portion of Figure 4. Assume that this circuit is designed to operate at 10 Hz, which is a typical value for a servo control. Let's further assume that the telescope has a rotational inertia  $J =$

12 slug-ft<sup>2</sup>.

$$\begin{aligned} \text{Since: } \omega_n^2 &= K_s/J \\ \text{then: } K_s &= (10 \cdot 2 \cdot \pi)^2 \cdot 12 \\ &= 47,300 \text{ ft-lb./rad} \end{aligned} \quad (5)$$

where:

$\omega_n$  = corner frequency of servo-loop  
 $K_s$  represents the servo stiffness

The preceding implies that an external torque of 10 ft-lb. will allow a movement of only  $10/47,300 = 0.0002$  rad, or 0.7 arc-min.

Now let's look at the low-frequency control loop portion of Figure 4. This will act as a vertical reference unit and ensure that the absolute pointing angle of the telescope matches the commanded (or target) angle. To accomplish this, a stable, long-term attitude reference must be provided.

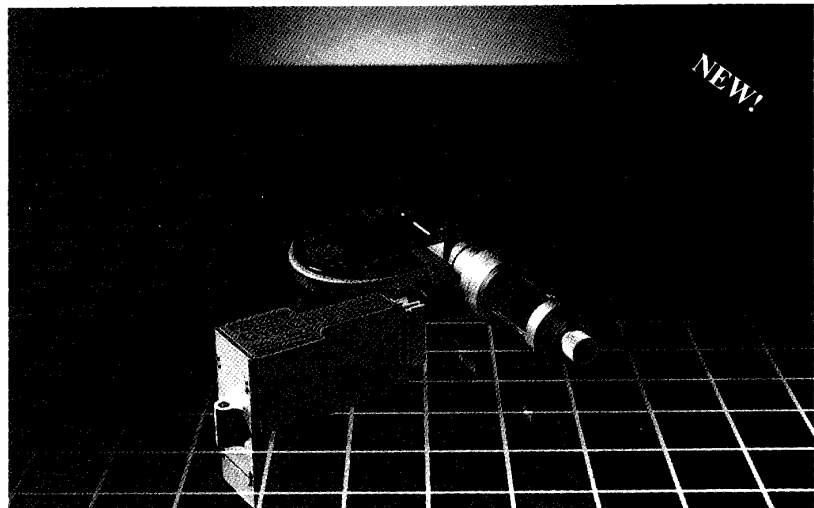
For most systems, gravity does the job quite nicely. A simple tilt sensor is always referenced to local gravity, and over a fairly narrow range it will behave linearly. To avoid coupling-in any high-frequency movements that are, by definition, not gravity related, this reference is part of a control loop with a time constant of typically 100 s. This allows the attitude reference to closely follow the typical platform motions you might find on most common mobile platforms, i.e., ships, trains, or planes.

In general, the loop will incorporate a proportional and differential control element that does not appear in the figure.

## SUMMARY

A new type of sensor has been developed that can add significantly to the capabilities of engineers and designers alike. Based on inertial-sensing principles, the quartz rate sensor provides a simple, reliable measurement of rotational velocity that can be used to instrument structures in new ways and gain a more in-depth insight into designs; to aid in short-term navigation of autonomous mobile platforms; and to allow for improved methods of stabilizing structures.

Scott D. Orlosky is Director for Commercial Business and Harold D. Morris is Chief Scientist, Systron Donner Inertial Division, a BEI Electronics Company, 2700 Systron Dr., Concord, CA 94518; 510-671-6601, fax 510-671-6647.



## Introducing a Solid-state Rate Sensor That Rivals the GyroChip.™ GyroChip II.

The makers of the GyroChip precision solid-state rotation sensor now offer the GyroChip II: a smaller, lighter, lower-cost rate sensor with all the precision manufacture and rugged reliability of the original.

The GyroChip II comes in two models: Standard, for use with battery systems (+12 V) and single-sided power supplies, and Low-noise, for use with double-sided ( $\pm 15$  V) supplies. Both models feature built-in power regulation and DC-in, DC-out operation.


The GyroChip II is ideal for:

- Servo Control
- Robotics
- Short Term Navigation
- GPS Augmentation
- Camera Stabilization
- Instrumentation

No matter how you use it, the GyroChip II gives you the assurance of quality that comes from our decades of experience in instrument design and manufacture.

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 If It Moves, GyroChip It!

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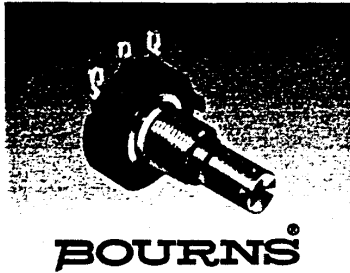
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## Bourns



### 3/4" (19MM) DIAMETER / CERMET OR CONDUCTIVE PLASTIC

- Single-turn (3851 and 3852)
- 3 -3/4-turn (3856)
- Minimal depth package
- Good resolution
- Linear and audio tapers
- Wide resistance range

FOR ORDERING INFORMATION SEE PAGE 258.

## Models 3851/3852/3856

Bourns® Panel Controls

	3851 Conductive Plastic Element	3852/3856 Cermet Element
<b>Initial Electrical Characteristics<sup>1</sup></b>		
Standard Resistance Range		
Linear Tapers (A, B, E, and H)	1K to 2.5 megohms	50 ohms to 5 megohms
audio Tapers (C, D, F, and G)	750 ohms to 2.5 megohms	1K ohms to 2.5 megohms
Resistance Tolerance	±20%	±10%
Zero Base Linearity	(B, D, & G tapers) ±20% (E taper) ±10%	(A, C, & F tapers) ±10% (H taper) ±5%
Independent Linearity	±10%	(A & H tapers) ±5%
Absolute Minimum Resistance	2 ohms maximum	2 ohms maximum
Continuity	Maintained for full mechanical angle	Maintained for full mechanical angle
Effective Electrical Angle	250° ±5°	250° ±5°
Contact Resistance Variation	±1%	±3% of total resistance or 3 ohms (whichever is greater)
Dielectric Withstanding Voltage	MIL-STD-202, Method 301	MIL-STD-202, Method 301
Sea Level	900 VAC minimum	900 VAC minimum
70,000 Feet	350 VAC minimum	350 VAC minimum
Insulation Resistance (500 VDC)	1,000 megohms minimum	1,000 megohms minimum
Power Rating (Voltage Limited By Power Dissipation or 316 VAC, Whichever Is Less)		
+70°C	(B & E tapers) 1 watt (D & G tapers) 0.5 watt	(A & H tapers) 2 watts (C & F tapers) 1 watt
+125°C	0 watt	0 watt
+150°C	0 watt	0 watt
Theoretical Resolution	Essentially infinite	Essentially infinite
<b>Environmental Characteristics<sup>1</sup></b>		
Storage Temperature Range	-65°C to +125°C	-65°C to +150°C
Temperature Coefficient		
Over Storage Temperature Range	±1,000PPM/°C	±150PPM/°C
Vibration	20G	20G
Total Resistance Shift	±2% maximum	±2% maximum
Voltage Ratio Shift	±5% maximum	±6% maximum
Shock	100G	100G
Total Resistance Shift	±2% maximum	±2% maximum
Voltage Ratio Shift	±5% maximum	±6% maximum
Load Life	1,000 hours	1,000 hours
Total Resistance Shift	±10% maximum	±3% maximum
Rotational Life (No Load)	100,000 cycles	50,000 cycles
Total Resistance Shift	±15% maximum	±5% or 5 ohms (whichever is greater)
Moisture Resistance	MIL-STD-202, Method 103, Condition B	MIL-STD-202, Method 103, Condition B
Total Resistance Shift	±10% maximum	±2% maximum
Insulation Resistance (500 VDC)	100 megohms minimum	100 megohms minimum
<b>Mechanical Characteristics<sup>1</sup></b>		
Shaft Torque	(A & B bushings) .05 to 6.0 oz.-in. (0.35 to 4.23 Ncm) (C & E bushings) 0.3 to 6.0 oz.-in. (0.21 to 4.23 Ncm)	3852 (A & B bushings) 0.5 to 6.0 oz.-in. (0.35 to 4.23 Ncm) (C & E bushings) 0.3 to 6.0 oz.-in. (0.21 to 4.23 Ncm) 3856 — 0.15 to 3.0 oz.-in. (0.11 to 2.12 Ncm)
Stop Strength	.5 in.-lb. (56.5 Ncm)	.5 in.-lb. (56.5 Ncm)
Mechanical Angle	280° ±5°	3852 — 280° ±5° 3856 — 1350° ±50°
Weight	30 grams maximum	30 grams maximum
Terminals	Printed circuit terminals or solder lugs	Printed circuit terminals or solder lugs
Marking	Manufacturer's trademark, wiring diagram, date code, resistance, manufacturer's part number manufacturer's part number	Manufacturer's trademark, wiring diagram, date code, resistance, manufacturer's part number resistance, manufacturer's part number

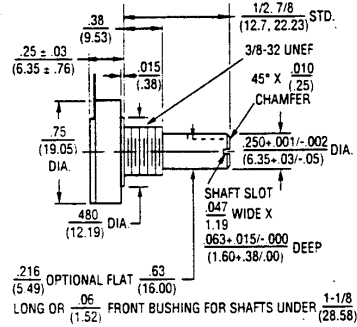
<sup>1</sup>At room ambient: +25°C nominal and 50% relative humidity nominal, except as noted  
Specifications are subject to change without notice.



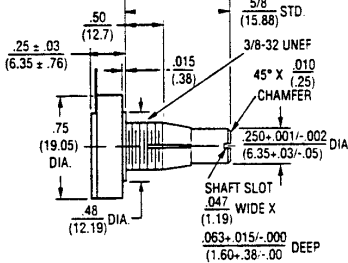
## DIMENSIONAL DRAWINGS AND TOLERANCES

### Model 3851/3852/3856

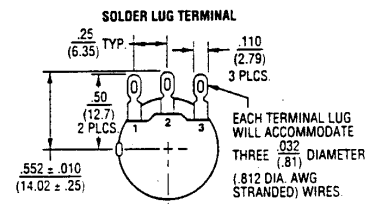
**3851A/3852A**



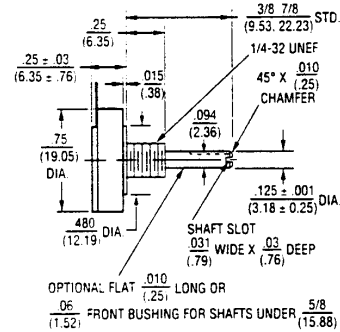
**3851B/3852B**



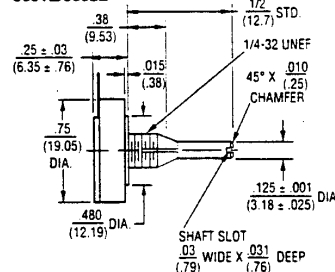
**Terminal Configuration**



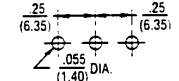
**3851C/3852C**



**3851E/3852E**

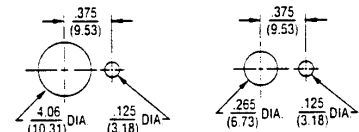


**SUGGESTED BOARD LAYOUT**

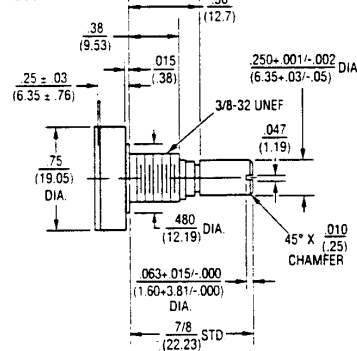


**3851/3852/3856**

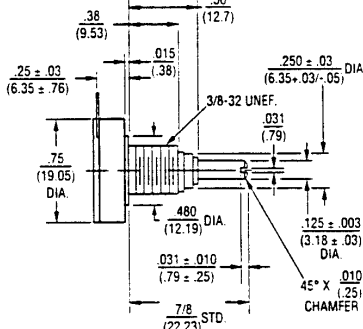
**A, B & H BUSHINGS**



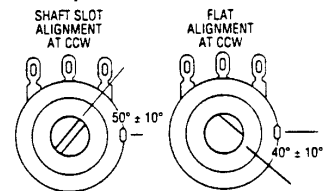
**3856A**



**3856H**

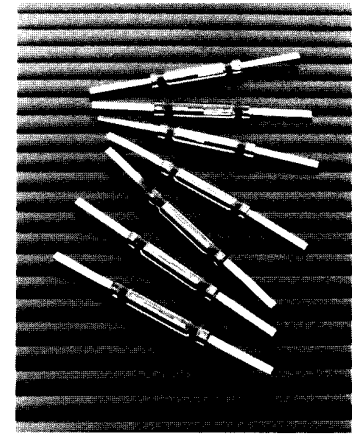


**Shaft End Detail  
3850 Family**



TOLERANCES EXCEPT AS NOTED:  
DECIMALS: .XXX ± .005 (127) XX ± .015 (38)  
FRACTIONS: ± 1/64  
ANGLE: ± 3°

# Reed Switch Specification



**SERIES FR2**

## Clare

Over the past three decades, billions of reed switches have been used in hundreds of applications. Operating in microseconds, they are quiet in operation and need little or no energy for actuation. When driven with an electromagnetic coil, reed switches can accumulate millions of fault-free operations at speeds up to 500 Hz continuously. Reed switches actuated by permanent magnets may lay poised for years, even in hostile environments, and operate perfectly when called upon.

Enhancements made by Clare to reed switch design and manufacturing processes have opened exciting new application possibilities. With more than 30 years experience in reed switch manufacturing, Clare is the world leader in glass-sealed contact technology. Clare DYAD reed switches deliver immediate improvements in end user yields and productivity.

The CLARE FR2 series reed switch is trademarked the DYAD. Unique features of the DYAD include:

- Patented glass to metal seal provides a stronger hermetic seal. Glass breakage is virtually eliminated.
- Sputtered ruthenium contacts provide stable contact resistance throughout life.
- Bifurcated contacts reduce bounce on closure offering faster momentary action and longer life.
- Flat glass dampens the kinetic energy of the blades on opening, virtually eliminating reclosure.
- Flat leads offer more reliable solder, weld, or crimp joints.
- Flat glass and flat leads also lend themselves to surface mount processing capability.

## Specifications

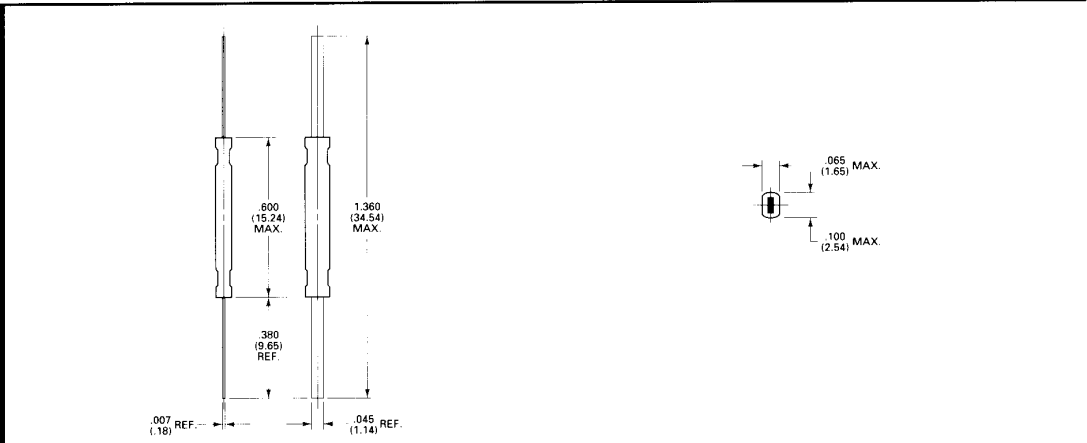
### Clare

PHYSICAL AND MECHANICAL REQUIREMENTS	
■ Contact Form	SPST, Form A (center gap)
■ Contact Material	Ruthenium
■ Standard Overall Length	1.360 inches (34.54mm)
■ Maximum Glass Length	0.600 inches (15.24mm)
■ Terminals*	Nickel iron alloy 52
■ Test Coil	NARM I test coil: See page 3 for details
CONTACT RATING	
■ Maximum Switching Power	10 VA
■ Maximum Switching Voltage	200 VDC, VAC
■ Maximum Switching Current	0.50 A
■ Maximum Continuous Carry Current	1.50 A
ELECTRICAL RATING	
■ Operate Sensitivity Available in Minimum 5 NI Ranges	5-45 NI
■ Maximum Initial Contact Resistance	150 milliohms
■ Minimum Dielectric Voltage	250 VDC
■ Maximum Capacitance	1.0 pF
■ Minimum Insulation Resistance	10 <sup>11</sup> Ohms
OPERATING CHARACTERISTICS	
■ Maximum Operate Time, Including Bounce	0.50 ms
■ Maximum Release Time	0.20 ms
■ Maximum Operating Frequency	500 Hz
■ Operating Temperature Range	-40°C to +125°C
■ Shock	100g, 11 ms, 1/2 sinewave
■ Vibration	20g, or .125" D.A., 10 - 5000 Hz
■ Solderability	As defined by MIL-STD-202 F, Method 208D
■ Resistance to Solvents	The reed switch operating characteristics shall not be affected by water wash, rinse procedures, the use of mild to semi-active fluxes or conformal coating processes.

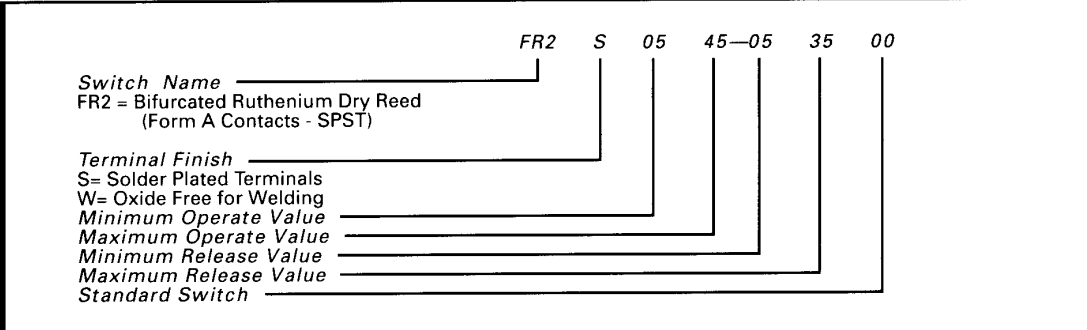
\* If the switch is to be soldered in place, a solder plated terminal finish should be specified.

Ordering Information

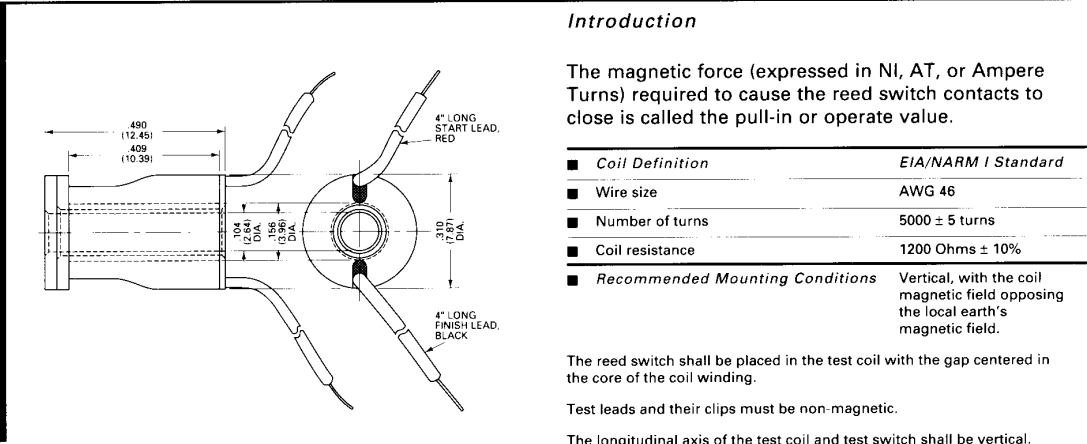
Dimensions



How to Order Clare Reed Switches



Standard Test Coil



Introduction

The magnetic force (expressed in NI, AT, or Ampere Turns) required to cause the reed switch contacts to close is called the pull-in or operate value.

■ Coil Definition	EIA/NARM I Standard
■ Wire size	AWG 46
■ Number of turns	5000 ± 5 turns
■ Coil resistance	1200 Ohms ± 10%
■ Recommended Mounting Conditions	Vertical, with the coil magnetic field opposing the local earth's magnetic field.

The reed switch shall be placed in the test coil with the gap centered in the core of the coil winding.

Test leads and their clips must be non-magnetic.

The longitudinal axis of the test coil and test switch shall be vertical.

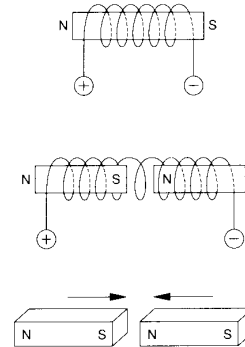
## Switch Actuation

### Clare

#### Operation of a Reed Switch Permanent Magnet and Electromagnetic Coil Actuation

The reed switch depends upon an induced magnetic field for its operation. Reed switches are activated by the presence of a magnetic field with sufficient flux to pull the reed blades together.

This can be accomplished by either using a permanent magnet—bringing the magnet close to the switch to turn it on—or by energizing a electromagnetic coil that is mounted around or near the switch. The balance of this page will review the actuating characteristics of a reed switch via these two methods.



#### Coil Actuation

The operation of a reed switch via an electromagnetic coil provides the designer with a method of actuation from a remote source. This is a very simple method of actuation.

When the reed switch is placed inside or close to a coil of wire and a current is passed through the coil, each lead of the reed switch becomes strongly magnetized. One end of the reed switch will become a north pole and the other a south pole. Because the reed blades overlap in the center of the glass housing, with a few thousandths of an inch separating the overlapping ends, each lead will have a north and south pole. The overlapping reed blades come together (close) when the

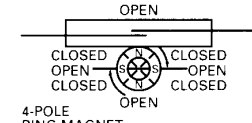
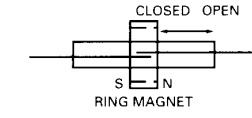
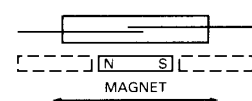
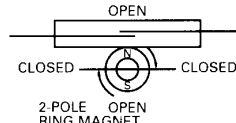
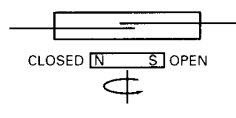
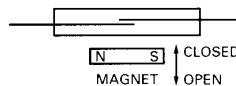
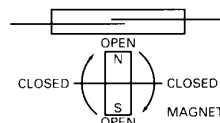
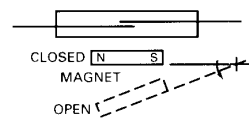
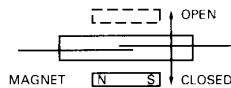
electrical current generates sufficient magnetic flux in the coil. When the current to the coil is turned off, the reed blades return to their open condition.

The efficiency of the reed switch actuation is largely dependent upon the coil. The size, shape, wire type, and the number of turns of wire on the coil determines its efficiency. In addition, the proximity of the switch to the coil determines the efficiency of the coil (ie, if the switch is placed inside or very close to the coil, the coil requires little current to actuate the switch. The farther the switch is from the coil, the more magnetic flux the coil must generate to cause switch closure). Two or more switches can be actuated by a single coil.

#### Permanent Magnet Actuation

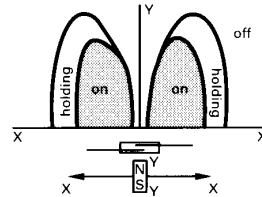
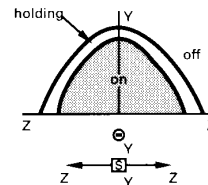
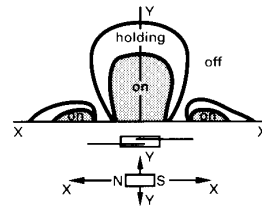
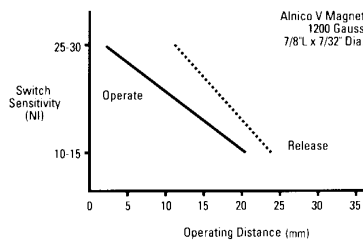
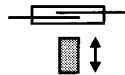
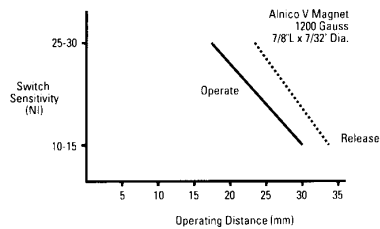
A permanent magnet is the most common means of operating the reed switch. As with a coil, to actuate the reed switch, a magnet and switch must be positioned within a specific proximity of each other. This distance is related to the sensitivity of the switch and the strength of the magnet. For the normally open reed

switch, when the magnetic field is close enough the contacts will close and when the magnetic field is taken away, the contacts will open. There are many ways to use a permanent magnet to actuate the reed switch. Below we have addressed the most popular techniques.



## Switch Actuation

### Permanent Magnet Actuation Distance (N. O. Contacts)



### Form B Reed Switch Actuation

#### Bias Actuation

Form B, N. C. contact actuation is achieved by Clare through the use of the standard Form A dry reed switch that is biased closed by mounting a permanent magnet to the switch housing. This magnet is located such that it keeps the switch in the on (or closed) condition.

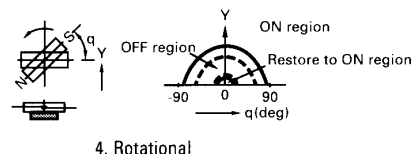
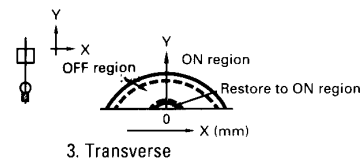
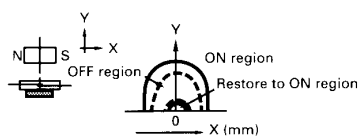
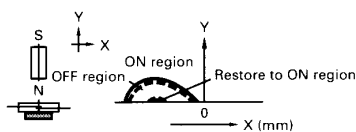
The switch is turned off (or opened) by bringing another magnet in the proximity of the switch/magnet assembly.

Note in the actuation charts shown below, that an on-off-on condition may occur if the proximity of the

actuating magnet is brought very close to the switch/magnet assembly. This condition is, of course, dependent upon the size and strength of the actuating magnet.

#### Magnets

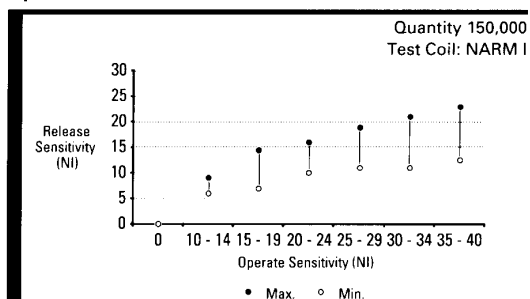
ALNICO V, ALNICO VIII, Ceramic and Barium ferrite are the most popular magnet materials used. The magnet type is usually chosen based on size, coercivity, cost, and temperature characteristics as defined by the application.



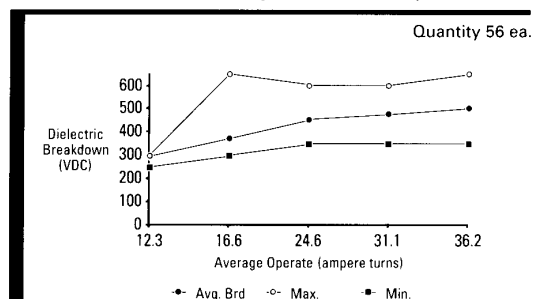
## Performance Data

### Clare

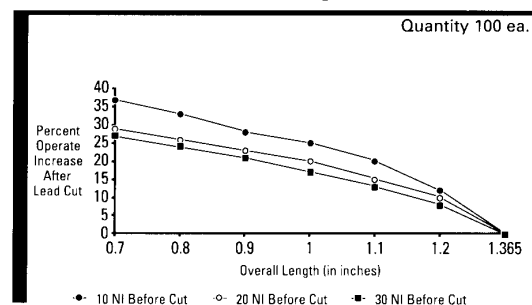
**Operate NI vs. Release NI**



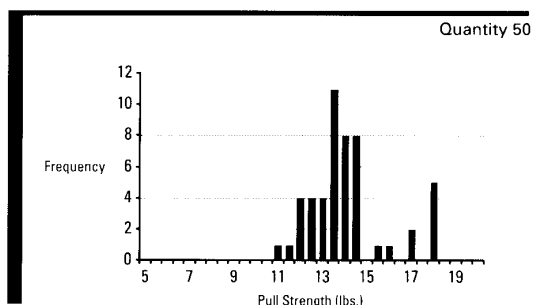
**Dielectric Breakdown vs. Operate Sensitivity**



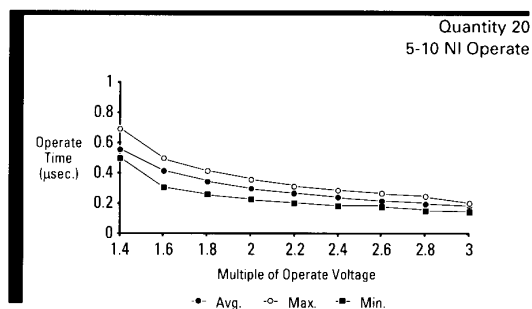
**Operate Shift After Lead Trimming**



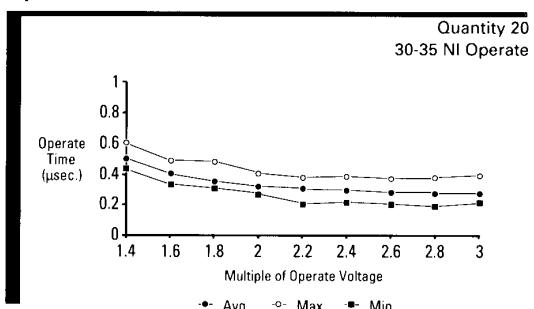
**Pull To Fracture Test Distribution**



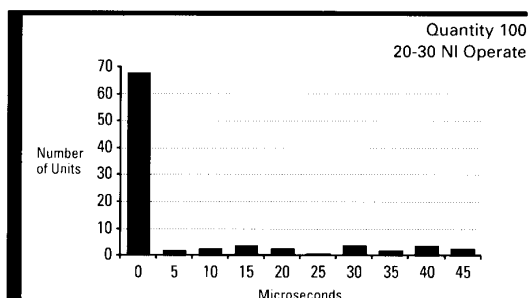
**Operate Time vs. Coil Drive**



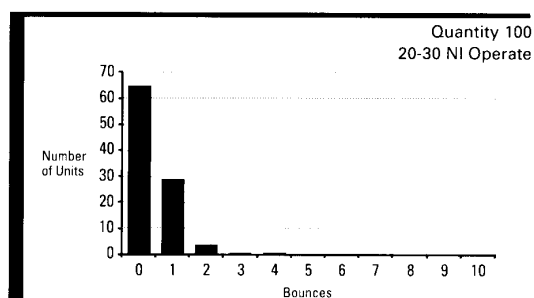
**Operate Time vs. Coil Drive**



**Bounce Time**



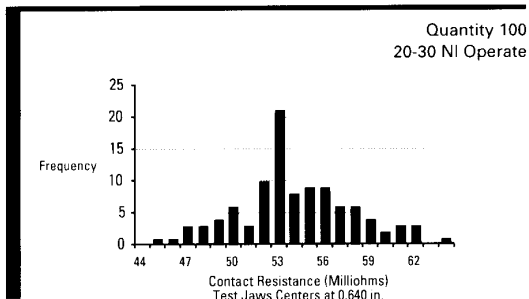
**Number of Bounces**



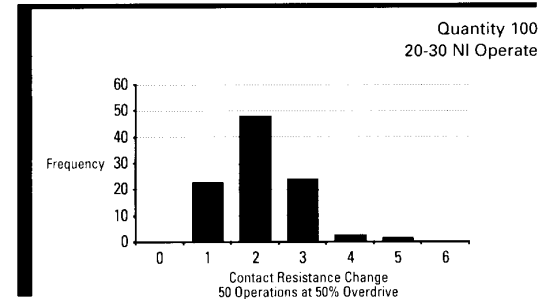


## Performance Data

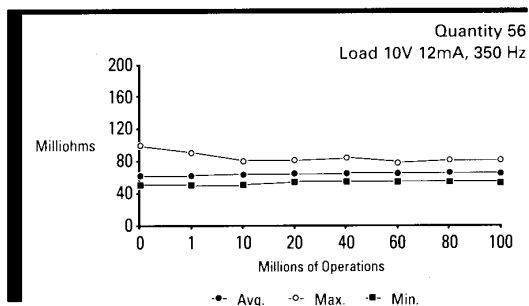
**Contact Resistance**



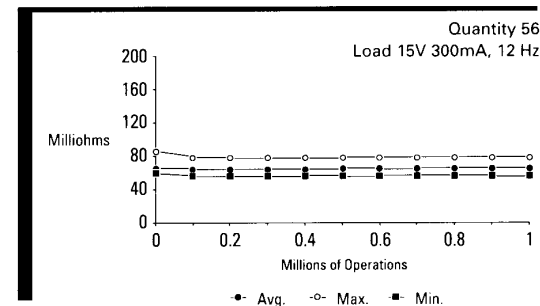
**Contact Resistance Stability**



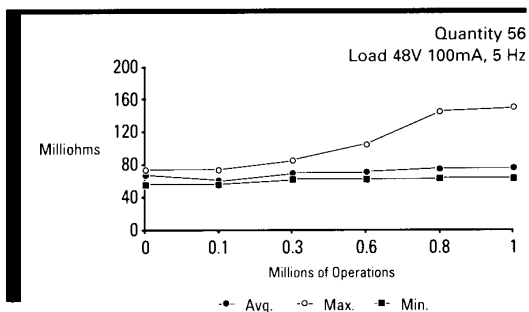
**Contact Resistance vs. No. of Operations**



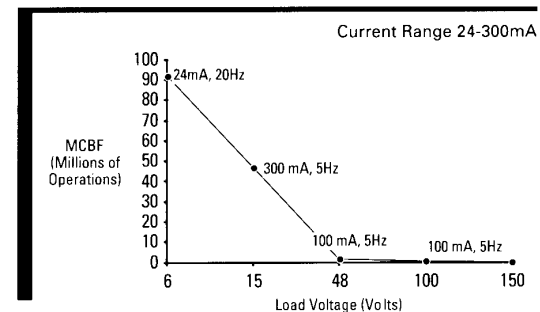
**Contact Resistance vs. No. of Operations**



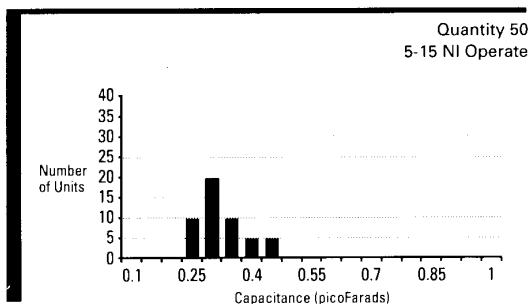
**Contact Resistance vs. No. of Operations**



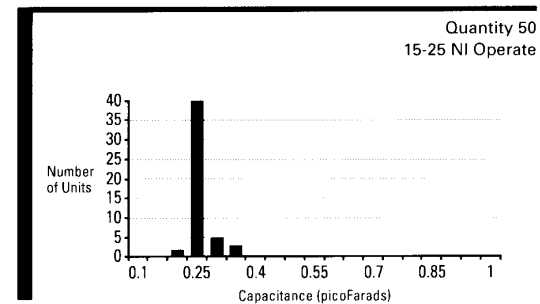
**Load Life**



**Capacitance Across Open Contacts**



**Capacitance Across Open Contacts**



## BATTERY CSB EVX 400 SERIES



### Features & Benefits

#### G2R 400 OXIDE

- ✓ Increases cycle life up to 122% versus standard sealed lead-acid technology.
- ✓ Standby float life is increased by 1.5 times when used in recommended optimum temperature range.
- ✓ Up to 50% greater resistance to grid growth under optimum temperature range.
- ✓ Provides hundreds to thousands of recharge cycles (cycle life is based on temperature and depth of discharge).
- ✓ Unrestricted U.S.A. shipment. Complies with IATA/ICAO Special Provision A67 for air transport. Recognized by DOT as "Dry Charge" 49 CFR 171-189 for surface transport. Classified per MG Amendment 27 as a non-hazardous material for water transport.
- ✓ EUROBAT classification: General Purpose.
- ✓ Cycle durability according to IEC 896, Part 2 equals 600.

#### Rechargeable

#### Immobilized Electrolyte

- ✓ Nonspillable, useable in any position.
- ✓ Maintenance free.
- ✓ Reduced internal resistance for superior performance.
- ✓ Extended shelf life.

#### Lead Calcium Cast Grid Construction

- ✓ Long service life.
- ✓ Increased current delivery for high-rate discharge.

#### Full Particle Tank Formation

- ✓ Cycle or standby use.
- ✓ 100% capacity 1st cycle.
- ✓ Uniform plate formation for consistent capacities.

#### 100% 2-Cycle Testing

- ✓ CSB-manufactured batteries are UL-recognized components under UL 924 CSB file number MH 14533. ISO 9001 Certified.

### Specifications & Characteristics

#### EVX-12170

NOMINAL VOLTAGE ..... 12 V

#### DIMENSIONS

- Container Height ..... 167 mm (6.57 inches)
- Length ..... 181 mm (7.13 inches)
- Width ..... 76.2 mm (3.0 inches)

WEIGHT ..... Approx. 6.14 Kg (13.50 lb.)

INTERNAL RESISTANCE ..... Approx. 15 mΩ

MAX. DISCHARGE CURRENT ..... 230 A (5 SEC)

STANDARD TERMINAL ..... Nut & Bolt

CONTAINER MATERIAL ..... General Grade ABS  
Also available: 94-V2(UL1778) flame retardant case

CONSTANT POWER WATT RATINGS Watts/Cell @ 25°C (77°F) to 1.70 V/Cell

60 min. ....	21.5 W/Cell	10 min. ....	75.0 W/Cell
30 min. ....	35.4 W/Cell	5 min. ....	111.0 W/Cell
15 min. ....	53.9 W/Cell		

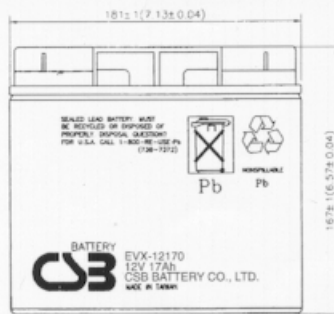
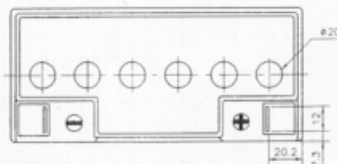
MAX. CHARGING CURRENT ..... 6.8 A

### Constant Power Watt Ratings (Watts/Battery @ 25°C, 77°F)

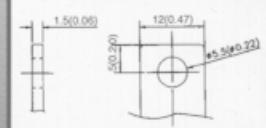
Final Voltage per Cell	1 min.	3 min.	5 min.	10 min.	15 min.	30 min.	60 min.	90 min.	3 hr.	5 hr.	8 hr.	10 hr.	20 hr.
1.80	650.0	609.0	569.0	432.0	304.0	199.0	121.0	89.2	51.0	33.3	22.1	18.3	9.87
1.70	777.0	711.0	665.0	449.0	323.0	212.0	129.0	95.0	54.3	35.5	23.6	19.5	10.5
1.67	826.0	753.0	678.0	454.0	329.0	215.0	132.0	96.7	55.3	36.1	24.0	19.8	10.7
1.60	842.0	766.0	690.0	462.0	344.0	225.0	137.0	101.0	57.7	37.7	25.1	20.7	11.2

### Dimensions

#### EVX-12170



### Terminal 5



Specifications subject to change without notification.



CSB Battery of America Corp.  
4018 Old Benbrook Rd., Fort Worth, Texas 76116 U.S.A.  
Tel: (817) 732-2258 • Tel: (800) 3CSB/USA • FAX: (817) 732-2019  
<http://www.csb-battery.com> • [csb@csb-battery.com](mailto:csb@csb-battery.com)



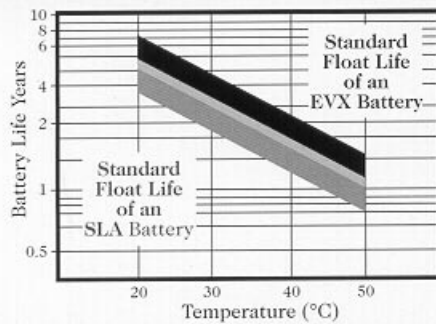
USA and Canada – [usasls@csb-battery.com](mailto:usasls@csb-battery.com)

Latin America – [latinsls@csb-battery.com](mailto:latinsls@csb-battery.com)

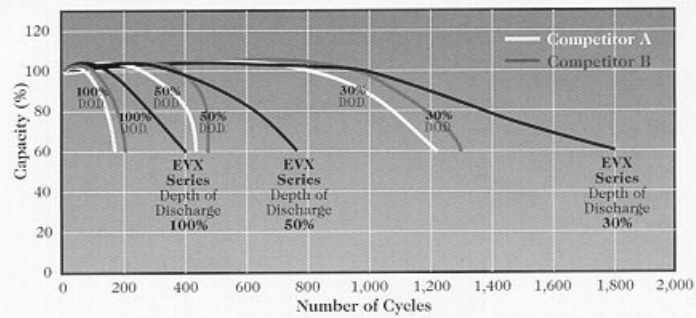
Europe – [eurosls@csb-battery.com](mailto:eurosls@csb-battery.com)

# THE 1999 FIRST ROBOTICS COMPETITION MANUAL

## Standby (Float) Life



## Cycle Life vs. Discharge Depth



## Discharge Current vs. Discharge Voltage

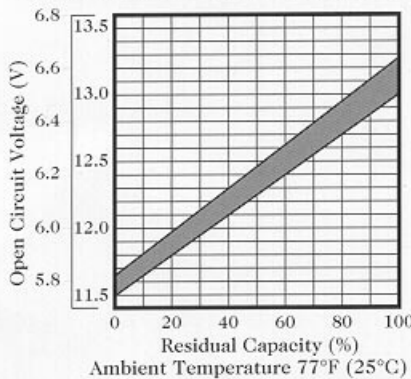
Discharge Current (A)	Final Discharge Voltage (V/Cell)
0.2C > (A)	1.75
0.2C ≤ (A) < 0.5	1.70
0.5C ≤ (A) < 1.0C	1.55
(A) ≥ 1.0C	1.30

## Optimum Temperature Ranges

Discharge:	5°-122°F	-15°-50°C
Charge:	41°-95°F	5°-35°C
Storage:	5°-104°F	-15°-40°C

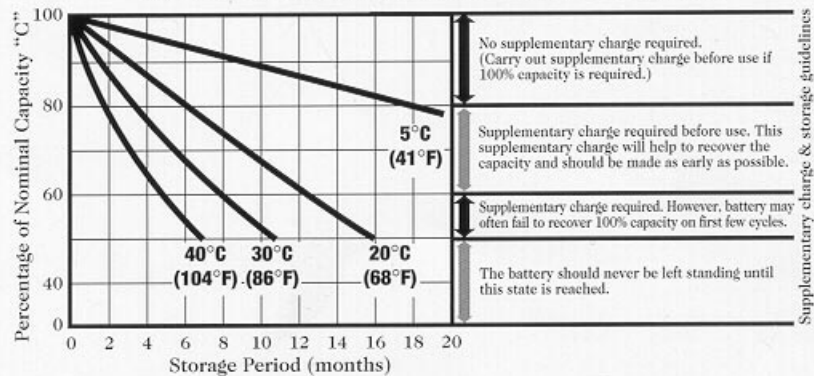
## Capacity

### OPEN CIRCUIT VOLTAGE vs. CAPACITY



## Storage

### BATTERY SELF-DISCHARGE AT VARIOUS TEMPERATURES



## Charging Procedures

	Applications	Charge Voltage (V/Cell)				Max. Current (A)	Charge Time	Max. Ripple Current
		Optimum Temp. Range	Temperature Compensation Required Outside Optimum Temperature Range	Set Point	Allowable Range			
EVX 12170	Cycle	5°C-35°C 41°F-95°F	Under 5°C Over 35°C	+5mV/°C/Cell -5mV/°C/Cell	2.45	2.45-2.50	0.4C Estimated 12-24 Hours	0.1 x C <sub>20</sub>
	Standby (Float)	5°C-35°C 41°F-95°F	Under 5°C Over 35°C	+3.3mV/°C/Cell -3.3mV/°C/Cell	2.275	2.25-2.30	0.4C Continuous	0.05 x C <sub>20</sub>

### Charging Precautions

- Always charge batteries in an open, well-ventilated area.
- Do not charge batteries near equipment which may produce sparks.
- Do not charge batteries in inverted position.
- Do not charge near an open flame.
- Do not use smoking materials in battery charging area.
- Electrolysis may cause hydrogen and oxygen to be released toward the end of a charging cycle or in the event the battery is overcharged. The combination of hydrogen and oxygen can result in an explosion if a spark or flame is introduced.

## Handling Precautions

- Never place or dispose of the battery near or in a fire.
- Never short the terminals.
- Never operate the battery in a gas-tight container.
- Never disassemble the battery.
- Never clean ABS battery cases with organic solvents.
- CSB batteries contain dilute sulfuric acid and in the event of contact to the skin or clothing, the exposed areas should be flushed generously with water. If contact with eyes or mucous membranes occurs, flush generously with water and seek medical attention.